WILSONS MILLS RD.
MUNSON TP

98

FIELD BOOK

360

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julian A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tabels see end of book.

Wilson Mills Road Sec 6.

Page 1

Wilson Mills Road Sec H.

page 32

Ditch levels of 5th ditch Pg 59 & 60
Wilson Mills Rd
opposite Dilka

Radii on turnouts int. Wilson Mills
& 306 Pg 61

Survey Fowlers Mills Rd Sec D & E
Pg 64

Elev. on Moccasin falls bridge
Pg 69 & 70 & 75-76

98

Traveled Rd with respect to & at
Mulberry & Fowlers Mills int. Pg 72

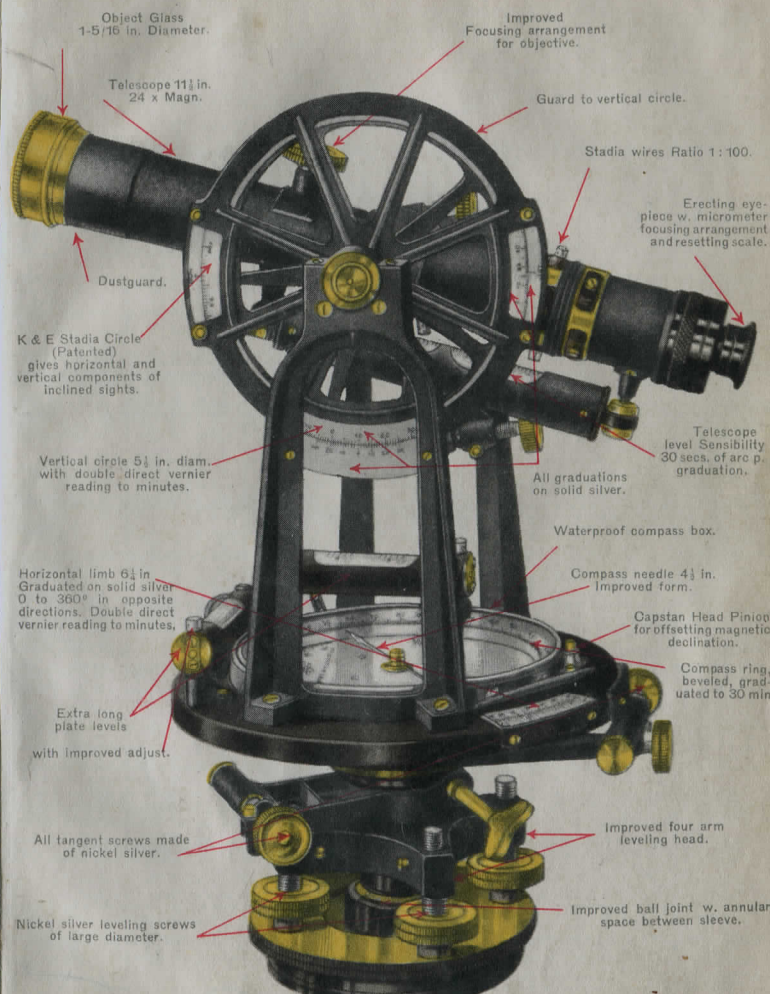
B.M. Levels from Auburn & Thwing Rd
int. to Moccasin falls bridge Pg 71 & 73

PP. 77-78
ELEVATIONS FOR N. END of MOCCASIN FALLS C.H. 108 9/1981

EXTRA FINE ENGINEERS' TRANSIT

No. 5060 S

KEUFFEL & ESSER CO., N.Y.



ALSO MADE WITH

INTERNAL FOCUSING TELESCOPE

PRACTICALLY DUST AND MOISTURE PROOF.

C.H. = 8 Wilsons Mills Rd.

1+12 Present 12" C.I.P. to be used for Driveway

NOTE: All Stakes Set 30' off ℄ of Rd. Unless Otherwise Indicated

0+0 1. Pipe fd. & Used — 12.0' — 13.0' — ℄ 1. Pipe fd. & Used
Iron Pin Set
East edge of Cone

April 15, 1930 (Cloudy) ⊙ S. Sold S. Merritt H. Barton

+36 ℄ 15' Drive — 9' — 16'-10" Cor Pipe (Very Poor Cond.)

+23 15" Cherry o 24' — 60°

1+12 — 11.5' — 8.5' — 12" C.I.P.

+98 E.E. STEALNS — 24.5 o C.E.I. Pole

+91 18" Apple o 21'

0+87 Wire Fence — 13'

+61 15" Apple o 20'

+11 T.P o Wire Fence — 15'

+01 12" Apple o — 25'

Wilsons Mills Rd.

Brush

90° 59' 30" — 140' — 34' — 6.

T.H. 105

Mun Sort Tp 1. Pin Set — ℄ Rd. Running So.

Chester Tp — 12' — Sta 0+0 — 1. Pin Fd. & Used.

Mon Box

Fred Wells

+58 T.P. ⊖ 15.5

6+56 P.L.

5+21 24.5 ○ C.E.I. Pole

4+40 T.P. ○ 13'

+80 24' ○ C.E.I. Pole

+38 16' ○ 24" Stump

3+34 16' ○ 10" Apple

+48 14' ○ 10" Stump

+38 24.5 ○ C.E.I. Pole

2+09 T.P. ⊖ 13'

+71 24" Apple ○ 34'

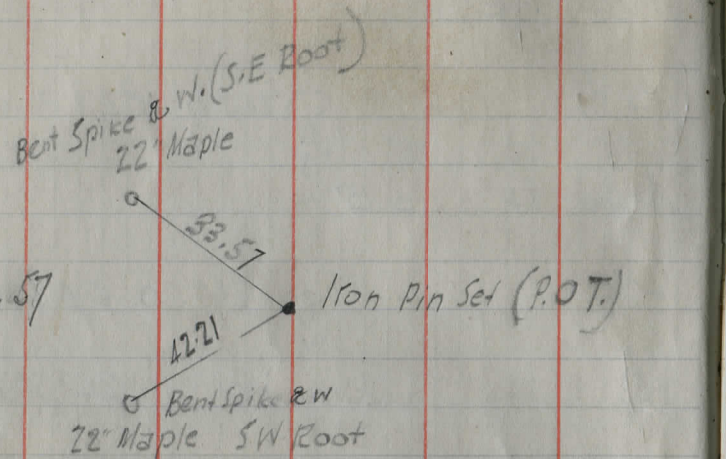
1½ St. Fr. Hse 25'

1+51 75'

E. E. Stearns

Wilsons Mills Rd. (60')

C. & M. VANEK



8+0 24.5 o C.E.I. Pole

+97 ℄ 16' Drive 16".12" C.I.P. (Fair Cond.)

10.5'

+88 22" Maple o 31'

+70 22" Maple o 31'

+56.47 P.O.T. Iron Pin Set

+40 16" Maple o 30'

1½-Story Fr. Hse 46' 68'

+29

7+27 22" Maple o 30'

+9 20" Maple o 30'

+74 8" Cherry o 15'

+69 30" Maple o 30'

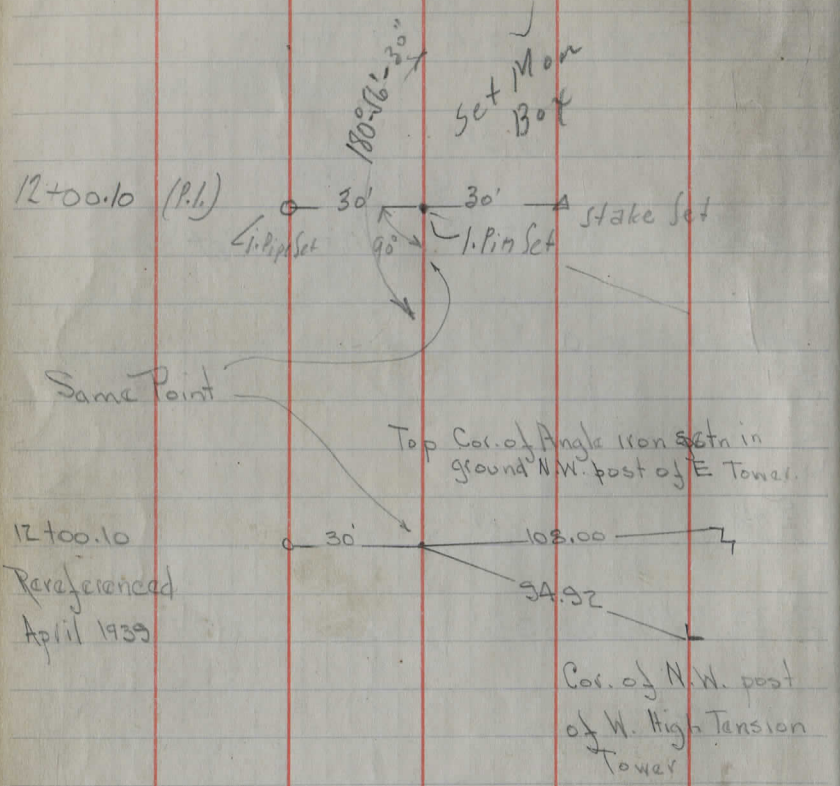
6+60 24.5' o C.E.I. Pole

F. Wells

Mills Rd.

Wilson

C & H VANAC



Brush

14+70 < 12' >

+63 23' ○ C.E.I. Pole

13+31 T.P ⊕ 17' (60')

12+23 25' ○ C.E.I Pole

+82 Wells Rd. 15' ○ 16" Apple

11+24 16' ○ 14" Apple

+95 T.P ⊕ 15' Mills

+81 24.5' ○ C.E.I Pole

+80 10' ○ 24" Stump

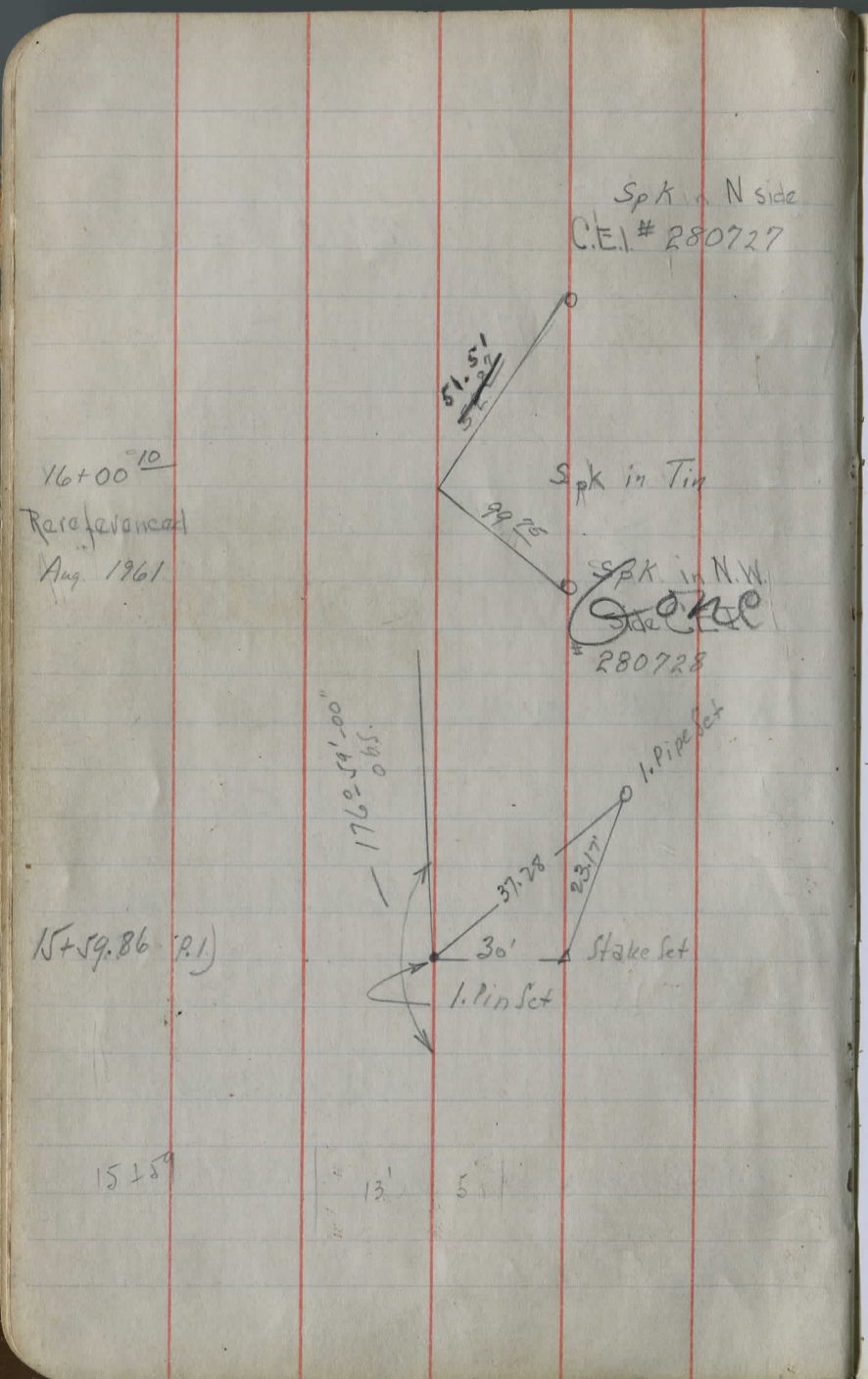
+38 Fred Wilsons 16' ○ 8" Apple

10+11 14' ○ 10" Apple

9+42 24.5 ○ C.E.I. Pole

8+42 T.P ⊕ 15'

PANEL W 8 C



+94 16' ○ 10" Apple

+45 Fred Wells 20' ○ C.E.I. Pole

+25 14" Stub ○ 16"

16+12 10" Cherry ○ 15'

+88 8" Cherry ○ 15'

+83 10" Cherry ○ 19'

+81 8" Elm ○ 14'

+77 12" Elm ○ 14'

+33 Wilsons (cont.) 11' ○ 12" Apple also Bag of Brush

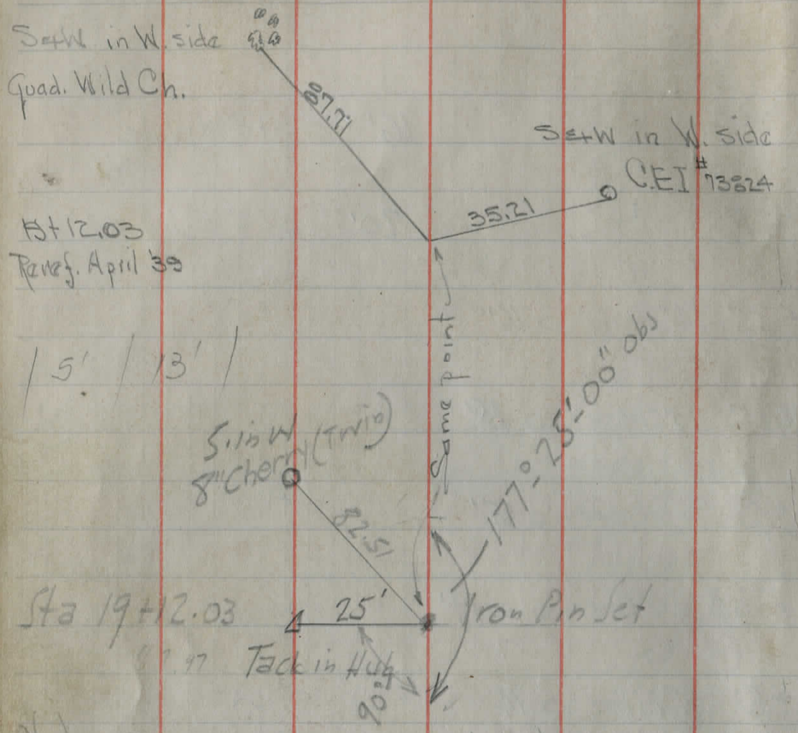
+27 30" Cherry ○ 15'

+15 8" Cherry ○ 14'

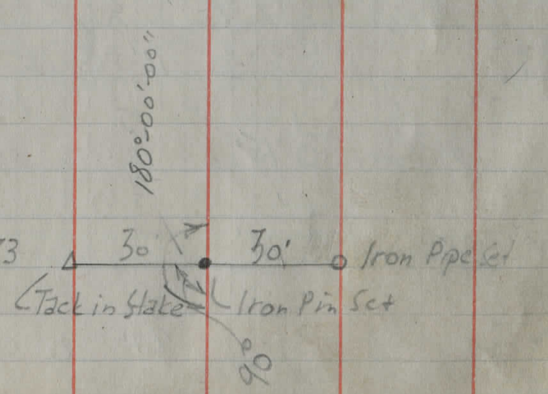
15+05 21' ○ C.E.I. Pole

(Continued from 160')

Wilsons Mills Rd



Note: See page 40 for relocation 19+12.03 to



April 17, 1930 (Cloudy)

S. Gold Jr.
S. Merritt
H. Barton

6

+90 Twin 8" o 27' Cherries

+90 10' o 8" Cherry

+89 19' o 18" Cherry

+89 145 o Property Line
Iron Pipe Fd.

+88 ← 10' × 12 → ←
End of Brush on Both Sides

+27 27' o C.E.I. Pole

19+12.03 • P.I. Iron Pin Set

18+96 10' o 10" Stump

+88 24' o C.E.I. Pole

+84 T.P. o 15.5'

+27 18' o 12" Apple

17+18.73 • P.O.T. Iron Pin Set

Fred Wells

℄ Wilsons Mills Rd

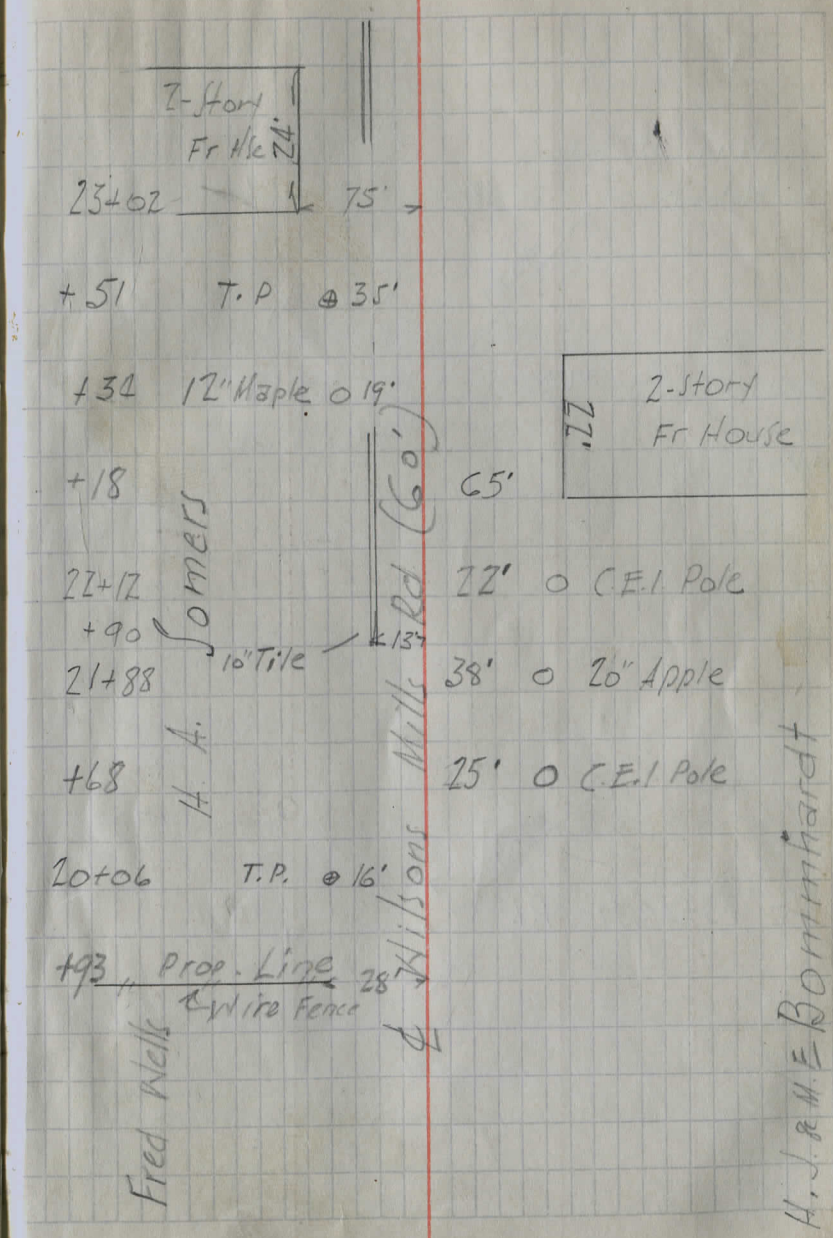
Cont Brush

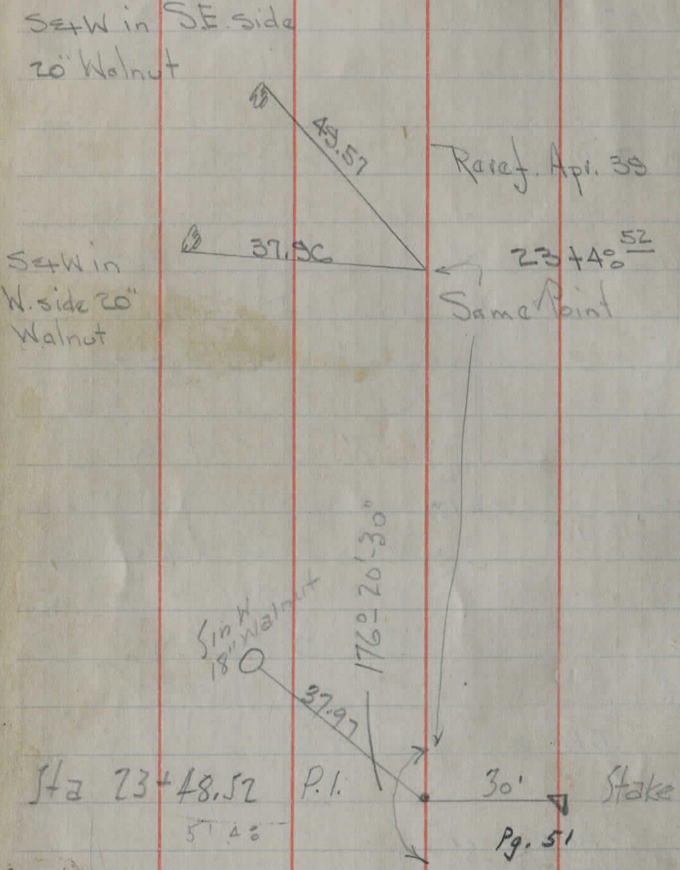
Brush

Cont.

H. J. & M. E. Bommhardt

C. & M. Vatrak


2-Story Fr Hse
24'
75'
23+62
+51 T.P. ⊕ 35'
+32 12" Maple ○ 19'
+18
22+17
+90
21+88
+68
20+06 T.P. ⊕ 16'
+93
Prop. Line
Wire Fence
28'
Somers Rd (60')
137'
10" Tile
H. A. Wilson Mills
Fred Wells
65'
22'
2-Story Fr House
22' ○ C.E.I Pole
38' ○ 20" Apple
25' ○ C.E.I Pole
H. J. & M. E. Bommhardt



Pt. is 6' from S. margin
+ 12' from N. margin

+55 10" Walnut o 21'

24+53 14" Walnut o 30'

+92 14" Walnut o 20'

+79 Beg. of Hedge 28'

+71 ℄ Gate (14')

+71 T. H Nash — 8' ℄ Drive ← 12'-8" C.I. Pipe

+58 Prop. Line 28' Wire Fence

+54 18" Walnut o 37'

+49 20' o C.E.I. Pole

+48.52 P.I. Iron Pin Set

+47 ℄ Drive 11' — 40'-10" Cor. I. Pipe (Fair Condition) +78' +38

+38 End of Tile 12

23+36 14" Walnut o 15'

Mills Rd.

Wilson

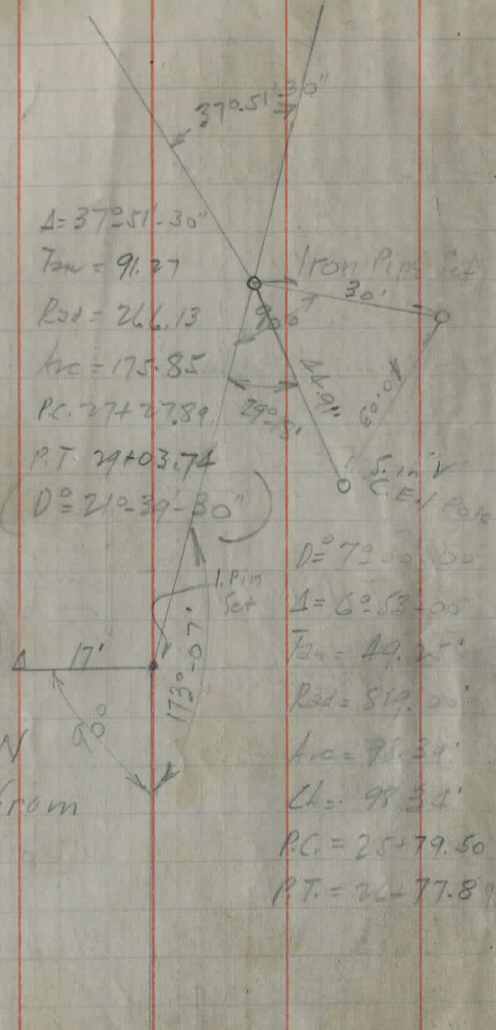
H. A. Somers

H. J. & M. E. Bomhardt

Wilsons Mills Rd

28+19.16 (P.I.)
see Pg. 52
New ℄

Δ = 37°-51'-30"
Tan = 91.27
Rad = 266.13
Arc = 175.85
P.C. 27+27.89
P.T. 29+03.74
(D° = 21°-39'-30")



26+28.75 (P.I.)

D° = 7°-00'-00"
Δ = 6°-53'-00"
Tan = 49.25'
Rad = 819.00'
Arc = 98.34'
Ch. = 98.34'
P.C. = 25+79.50
P.T. = 26+77.89

Pt. 2' from N margin 16' from S. margin.

2819.16
2628.75
190.41

April 22 1950

S. Gold Jr
S. Merritt
H. Barton

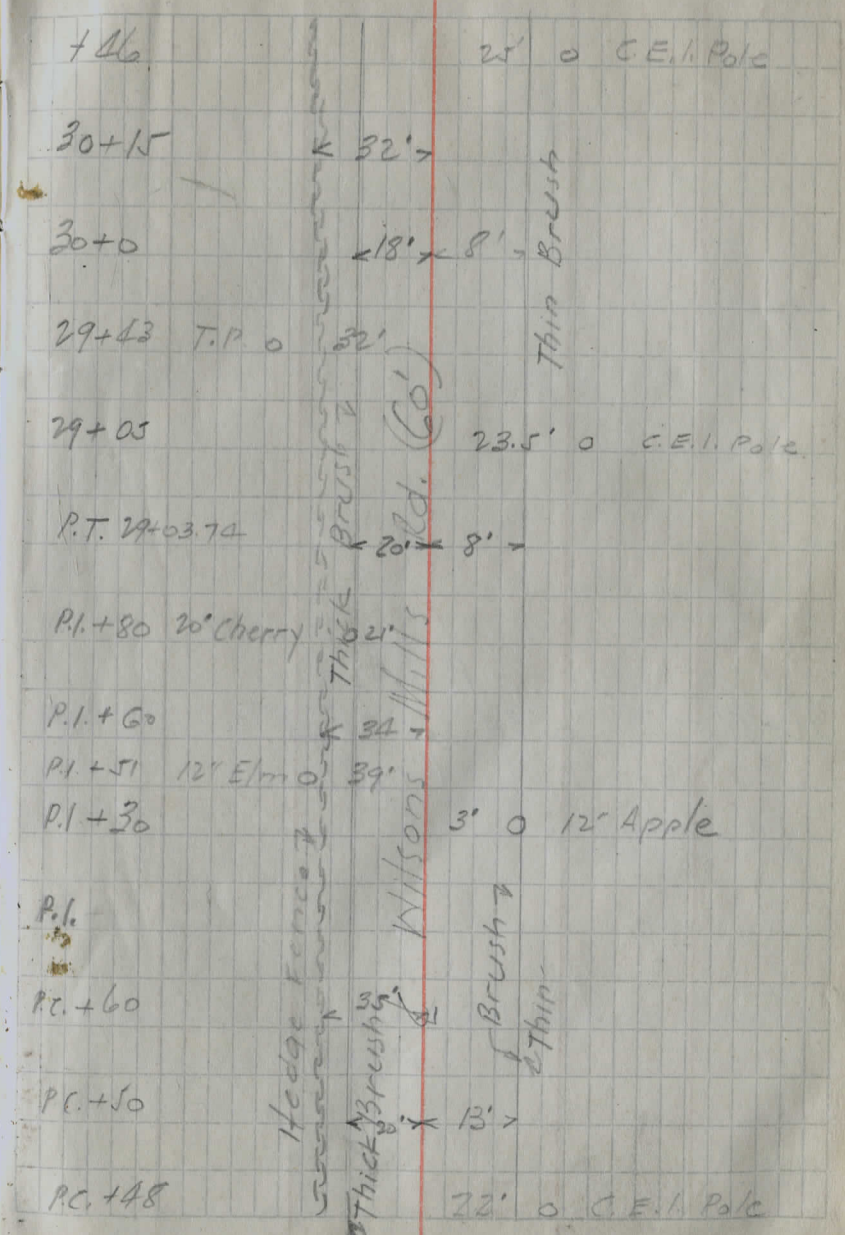
(9)

+32 T.P. o 34'
P.C. +32 ← 30
P.C. +13 8" Elms 22'
P.C. 27+27.89 ← 22' ← 10' ← 10'
27+0 13'
P.T. 26+77.89 ← 20' ← 5'
P.I. 26+28.75 ← 20' Iron Pin Set
26+0 ← 20'
+90 24" Maple o 14'
+27 T.P. & o 22.5
25+0 ← 25'
24+85 26' o C.E.I. Pole
24+62 12' Beg. of Brush

T. H. N. J. — (Thick Brush) — Hedge Brush — Wilsons Mills Rd. 60' — Brush — Brush

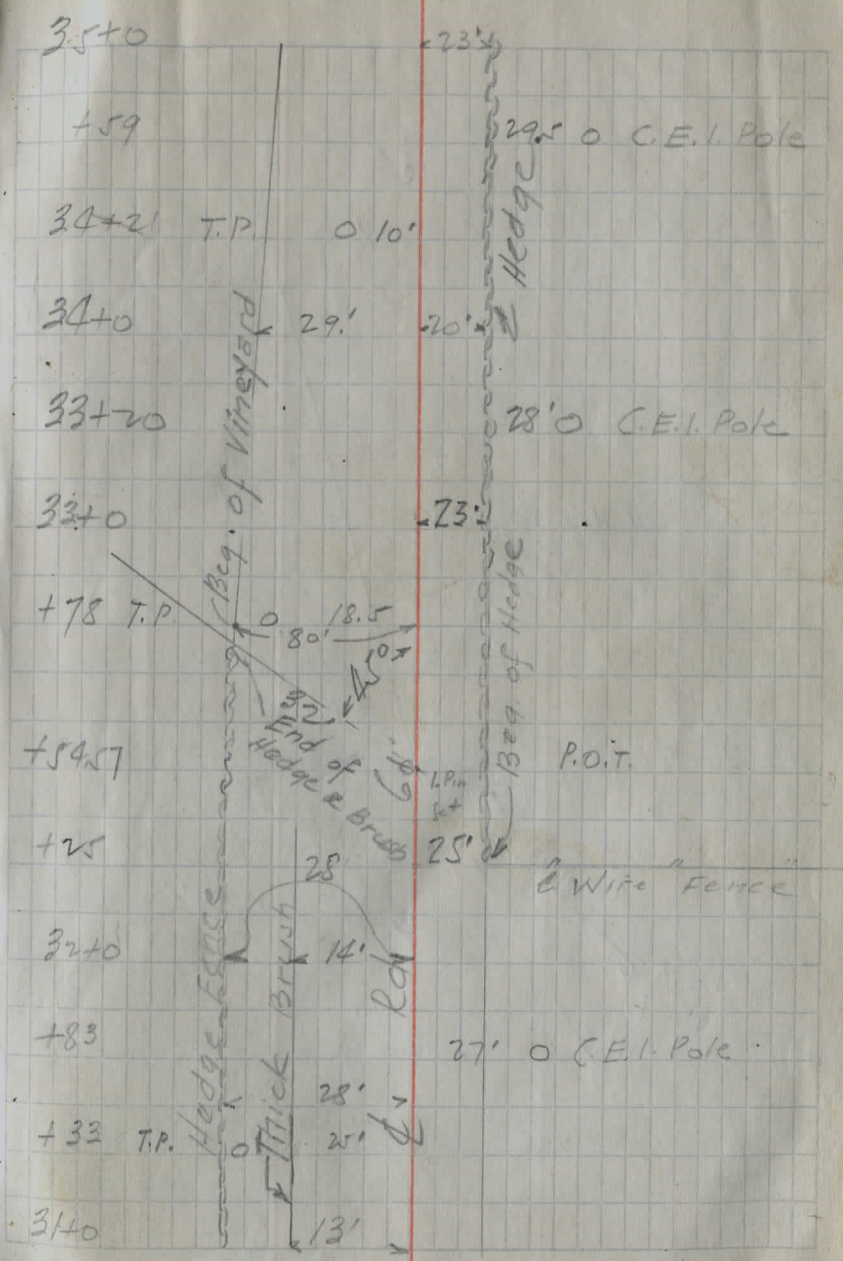
H. J. & H. E. Bornabret

Note Topography Taken on Tangents


7+46
25' ○ C.E.I. Pole
30+15
32'
30+0
18'
8'
Thin Brush
29+43 T.P. ○ 32'
29+03
23.5' ○ C.E.I. Pole
P.T. 29+03.74
20'
8'
Thick Brush & Trees (60')
P.I. +80 20" Cherry
21'
P.I. +60
34'
P.I. +51 12" Elm ○ 39'
P.I. +30
3' ○ 12" Apple
Wilsons Mills Rd.
P.I.
P.C. +60
Hedge Fence & Trees
Thick Brush
Brush & Thin
P.C. +30
13'
P.C. +48
22' ○ C.E.I. Pole

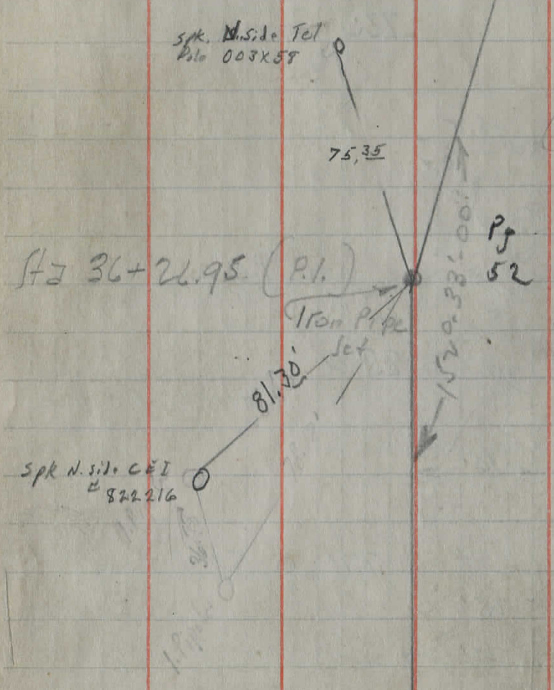
P.O.T.

32+54.57 — 30' — 30' — Tack in Stake
Iron Pipe set — Iron Pin set



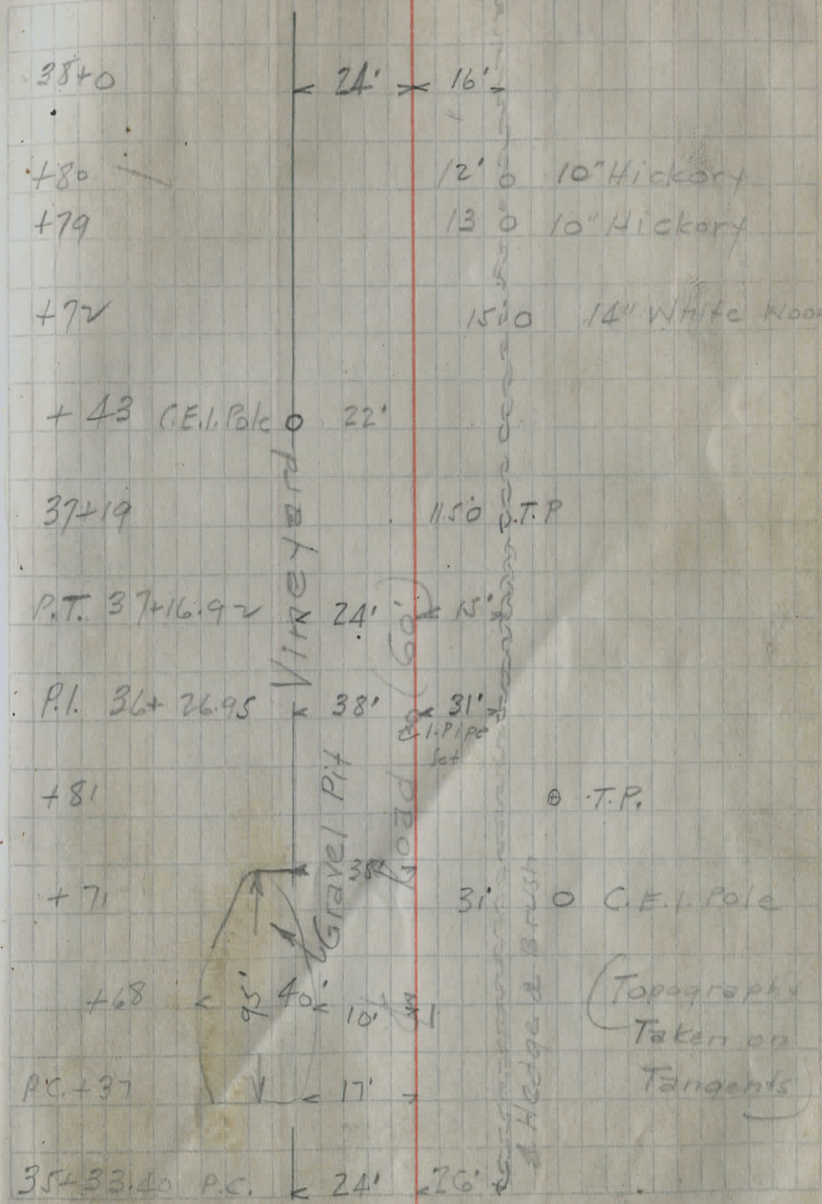
36-26.95
29 03.74
723.21
91.27
814.48

27-27
152-33



(D = 15°00'00")
Δ = 27°27'00"
Tan = 93.55'
Rad = 383.06
Arc = 183.52
Ch. = 181.7
P.C. 35+33.40
P.I. 36+26.95
P.T. 37+16.92

J Gold Jr
J. Merrett
A. Barton



Wilson's Mills Rd

April 24, 1930 (Cold)

S. Gold Jr
S. Merritt
H. Barton

13

22' ← Hedge
19.5' Wire Fence
I. Pipe Fd. ℄ P.L.

+46

+42 22' ○ C.E.I. Pole

+37 ℄ 12' Dr.

+27 C.E.I. Pole ○ 22'

+20 22' ○ 16" Walnut

40+08 60" Willow ○ 30'

+53 60' 17' ○ 8" Cherry

Barn 34' 115'

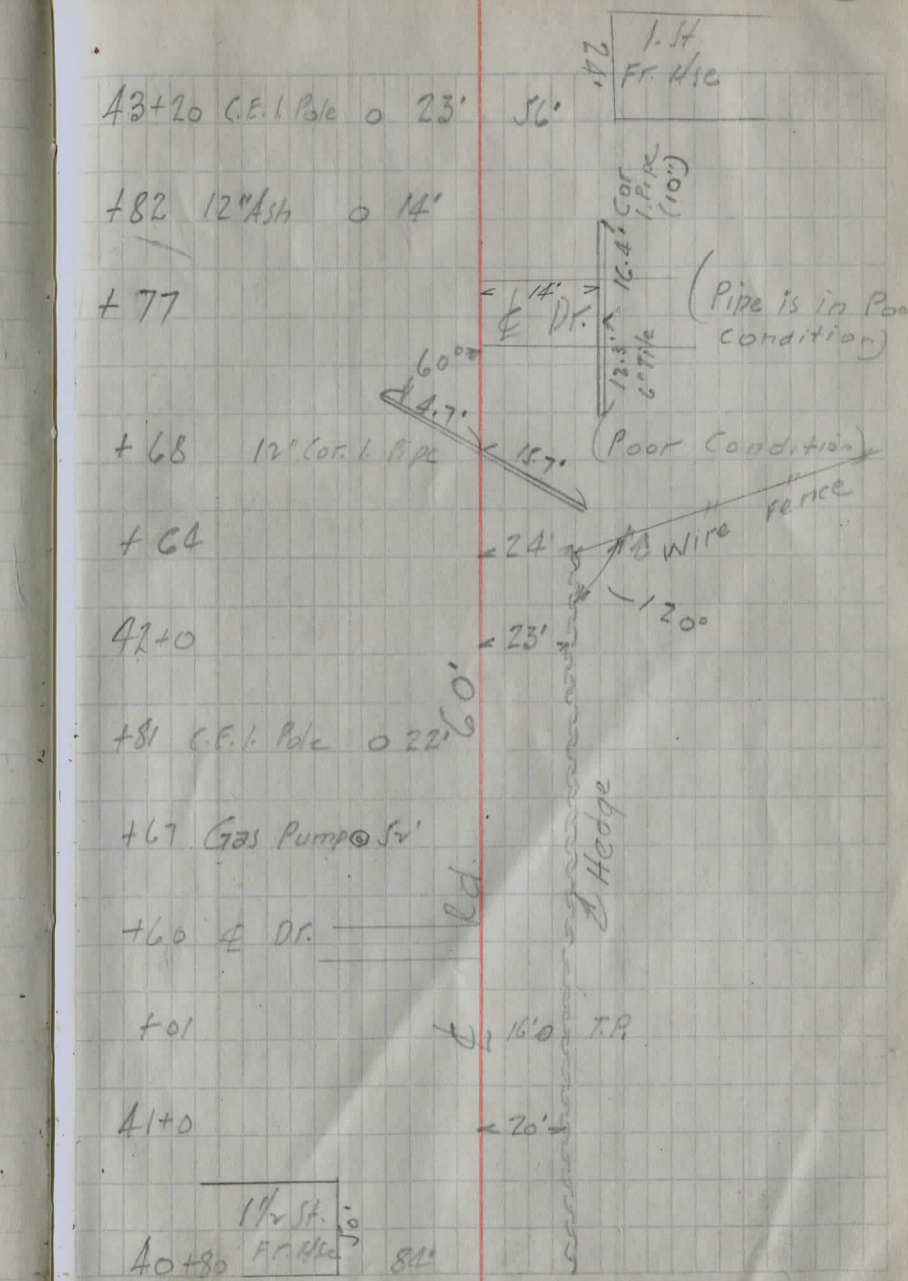
+48

39+45 Iron Pipe Fd.
208' Prop. Line
12'

39+05 End of Vineyard ← 24'

+81 C.E.I. Pole ○ 22.5'

38+79 Brush & Hedge 12' ⊕ T.P.

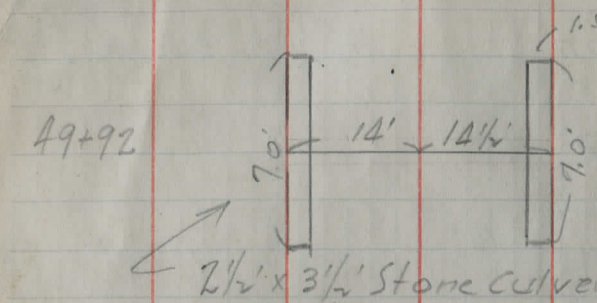

43+20 C.E.I. Pole o 23' 56'
+82 12" Ash o 14'
+77
+68 12" Cor. I. Pipe
+64
41+0
+81 C.E.I. Pole o 22'
+67 Gas Pump @ 5'
+60 ℄ Dr.
+01
41+0
40+80
1.5 St. Fr. Hse
24'
Cor. I. Pipe (10")
16.4'
℄ Dr.
14'
12.3'
6" Tile
(Pipe is in Poor condition)
60°
4.7'
15.7'
(Poor Condition)
fence
2 Wire
120°
24'
23'
60'
Hedge
Rd.
16'0 T.P.
20'
1½ St. Fr. Hse
50'
84'

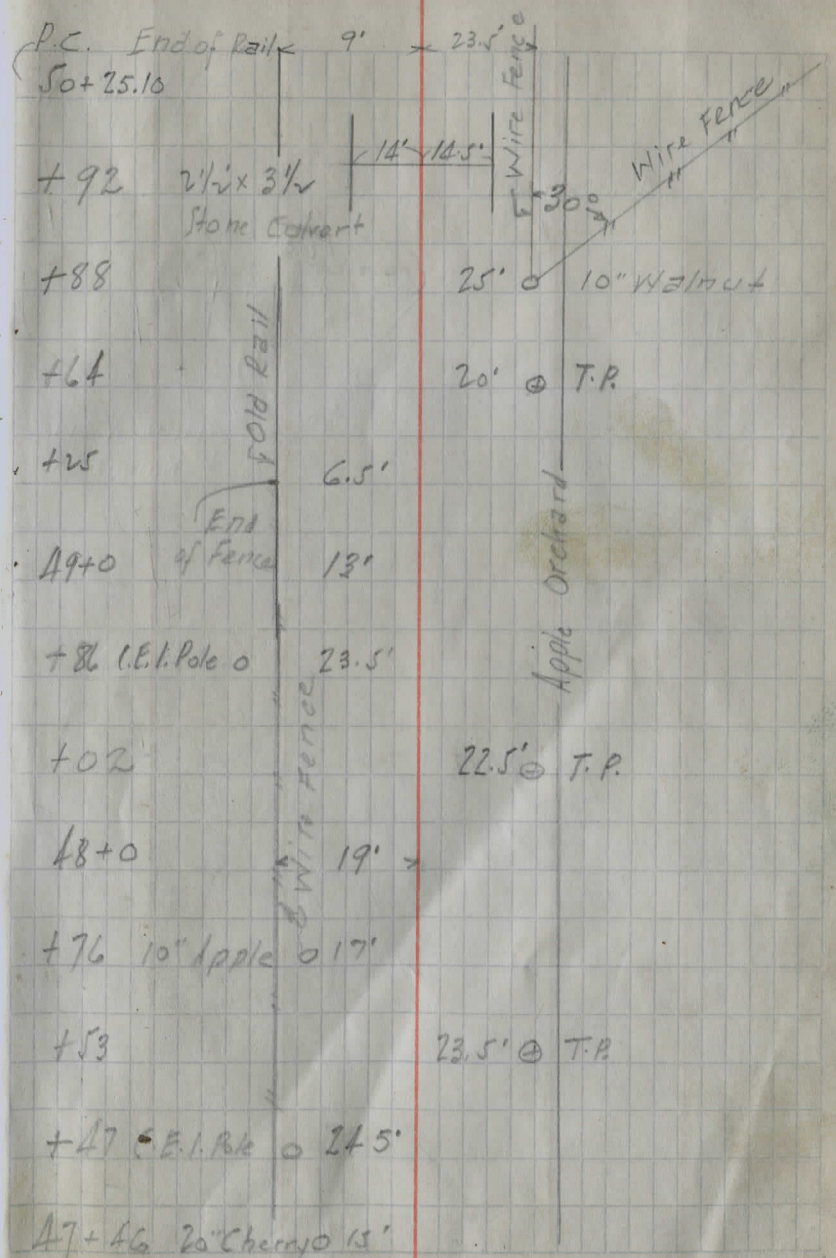
47+26.91 — 20' — 30' — Tack in Stake
Zi. Pipe Set — Zi. Pin Set — (P.O.T.)

50 80.75
47 26.91
353.84

+26.91 P.O.T. — Iron Pin Set
+08 20" Asm ⊙ 22'
47+0 — 18'
+52 30" Ash ⊙ 16'
+34 Wire Fence — 20'
+22 ⊠ Prop. Line
46+01 C.E.I. Pole ⊙ 23.5'
+90 — 40'
+43 — 22' ⊙ T.P.
45+0 — 34'
+62 — 31'
+42 C.E.I. Pole ⊙ 24'
44+22 — 42'
43+35 — 21' ⊙ T.P.

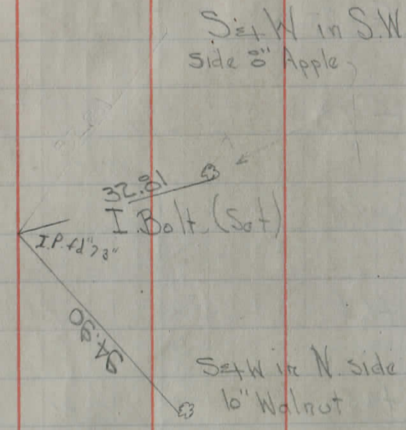
Wire Fence
Apple Orchard
39'
(60')
Apple Orchard
Pear Orchard


49+92
1.5'
7.0'
14'
14½'
7.0'
2½' x 3½' Stone Culvert
So End (14") is in Poor Condition


P.C. 50+25.16
End of Rail
9'
23.5'
Wire Fence
14'
14.5'
Wire Fence
30°
+92
2½' x 3½' Stone Culvert
+88
25' ⊙ 10" Walnut
+64
20' ⊙ T.P.
+45
Old Rail
6.5'
End of Fence
49+0
13'
+86 C.E.I. Pole ○
23.5'
Apple Orchard
+02
22.5' ⊙ T.P.
48+0
Wire Fence
19'
+76 10" Apple ○ 17'
+53
23.5' ⊙ T.P.
+47 C.E.I. Pole ○ 24.5'
47+46 20" Cherry ○ 15'

Wilsons Mills Rd

$\Delta = 6°-34'-30''$ Lt



50+80 75
Reset Apr. '39

D = 6°-00'
Δ = 6° 36'-30"
Tan = 55.15
Rad = 955.37
Arc = 110.19
Ch = 110.12

P.C. 50+25.10
P.T. 51+35.29
E = 1.59

50+80.75 (P.I.) — 30' — ℄ — 30' — Tack in Gate
I. Pipe Set — ℄ I. Pipe Set

April 26, 1930 (Fair)

J. Gold Jr.
J. Merritt
A. Barton

17

53+0	1½ Story Fr. Hse. 28'		25'
+62		93'	35'
+71	C.E.I. Pole	o 23.5'	
+31			21' ⊕ T.P.
52+0			21'
+99	12" Apple	o 21.5'	
51+56	C.E.I. Pole	o 26.5'	
P.T. 51+35.29			19'
P.I.+14	12" Apple	o 19' (Go)	30'
P.I.	Iron Pipe Set	℄	18'
P.C.+21	Wire fence 90°	23'	℄ Rd
P.C.+08	C.E.I. Pole	o 24'	
P.C.+08			22' o C.E.I. Brace
P.C.+0	18" Ash	o 22'	

Wire Fence
Apple Orchard

Note: Topography taken on Tangents

+21 48° ○ 12" Maple

30' 1½-St. Fr Hse

+14 ← 67'

+10 55° ○ 20" Locust

16'-10" Cor. I. Pipe (Poor
22'-10" V. Pipe (Fair)

55+09 38' ← 15' → ℄ Drive

+94 ← 36' → End of Orchard

+51 19.5 ⊙ T.P.

+ 28 10" Cor. I. Pipe 16' (60') (Good condition)

+11 28° ○ C.E.I. Brace

+10 Rd. ← 29' → End of Fence

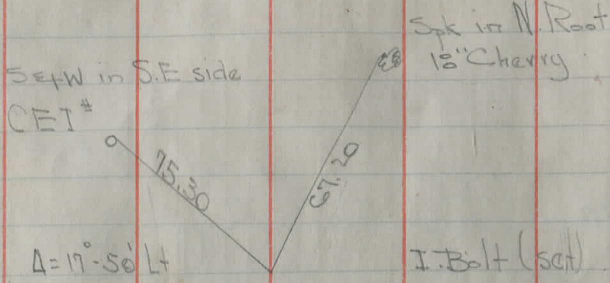
54+09 ⊂E.I. Pole ○ 19.5'

+64 1200 8" V.P.

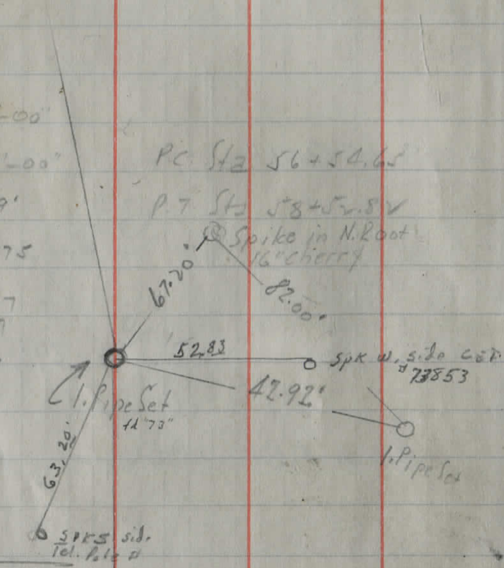
16' 14'

+63 6" Tile ← 10' → 4"

53+03 ℄ Drive



57+54.27 Δ=17°-50' Lt
Reset Apr '39



D° = 9°-00'-00"
Δ = 17°-49'-00"
Tan = 99.89'
R = 637.275
Arc = 198.17
Ch = 197.37

P.C. Sta 56+54.65
P.T. Sta 58+52.82

Sta 57+54.54 P.I.

5754.54	674.40
5135.29	5073.66
619.25	5748.06
55.15	
674.40	
4720.30	
5394.70	

+92 — 14' o 18" Pine

2-St Fr Hse — 73' .02

+91

+71 — 44' o 16" Pine

+64 C.E.I. Pole o 24.5

59+0

58+58

+67 C.E.I. Pole o 25'

P.I. +64 — 30' o 16" Cherry

P.I. +60 — 19' ⊕ T.P.

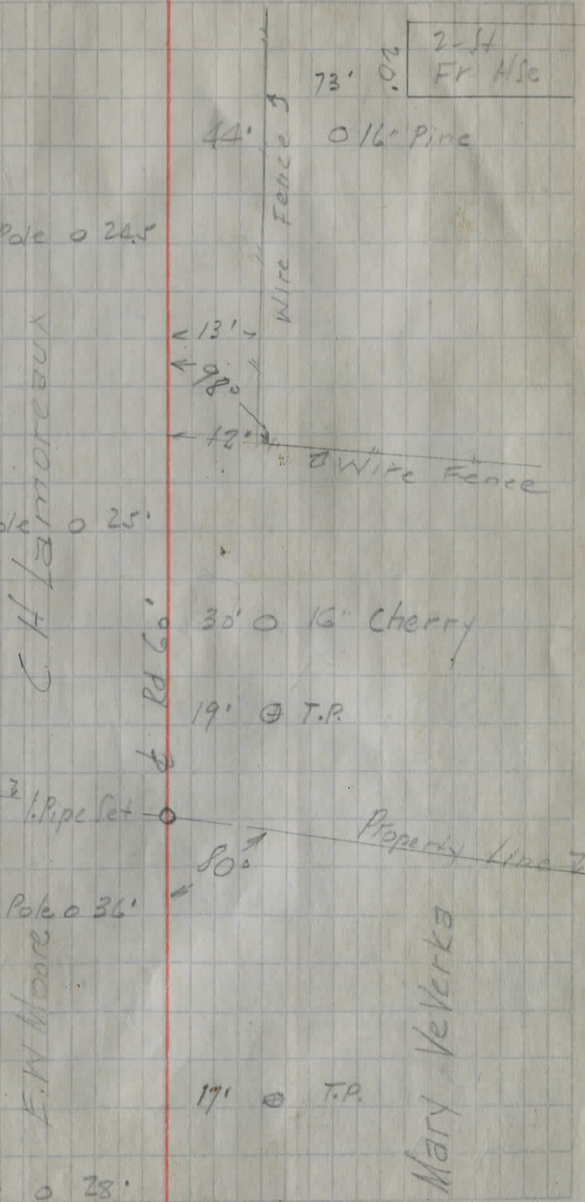
P.I. 57+54.54 I. Pipe Set

P.C. +22 C.E.I. Pole o 36'

P.C. 56 54.65

56+05 — 17' ⊕ T.P.

55+53 C.E.I. Pole o 28'



65+30 C.E.I. Pole o 24'

64+02

63+87 C.E.I. Pole o 24'

+46 C.E.I. Pole o 24'

62+13

+37

61+04 C.E.I. Pole o 24.5'

+85

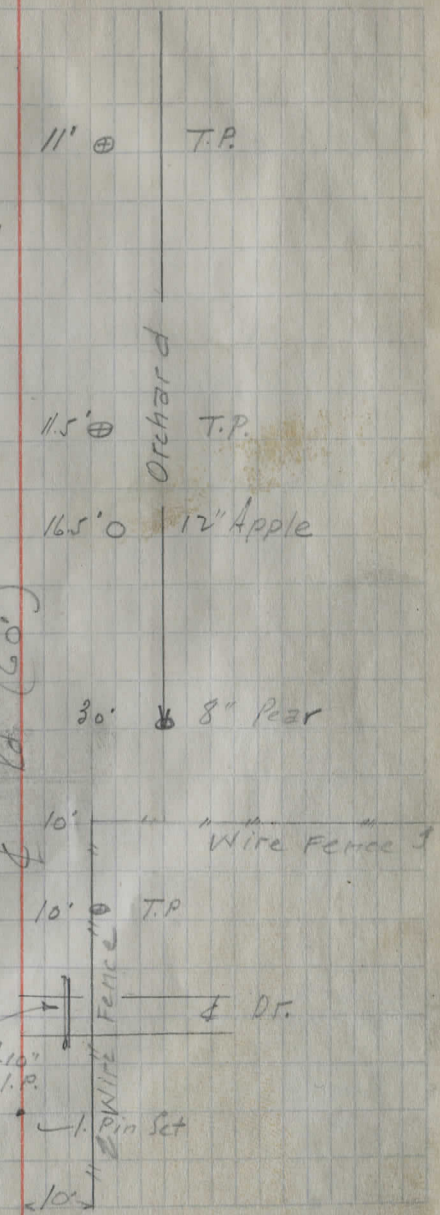
+83

+28

+19

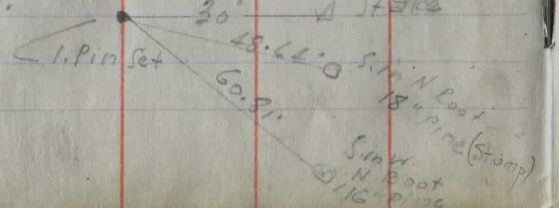
60+10.33 P.O.T.

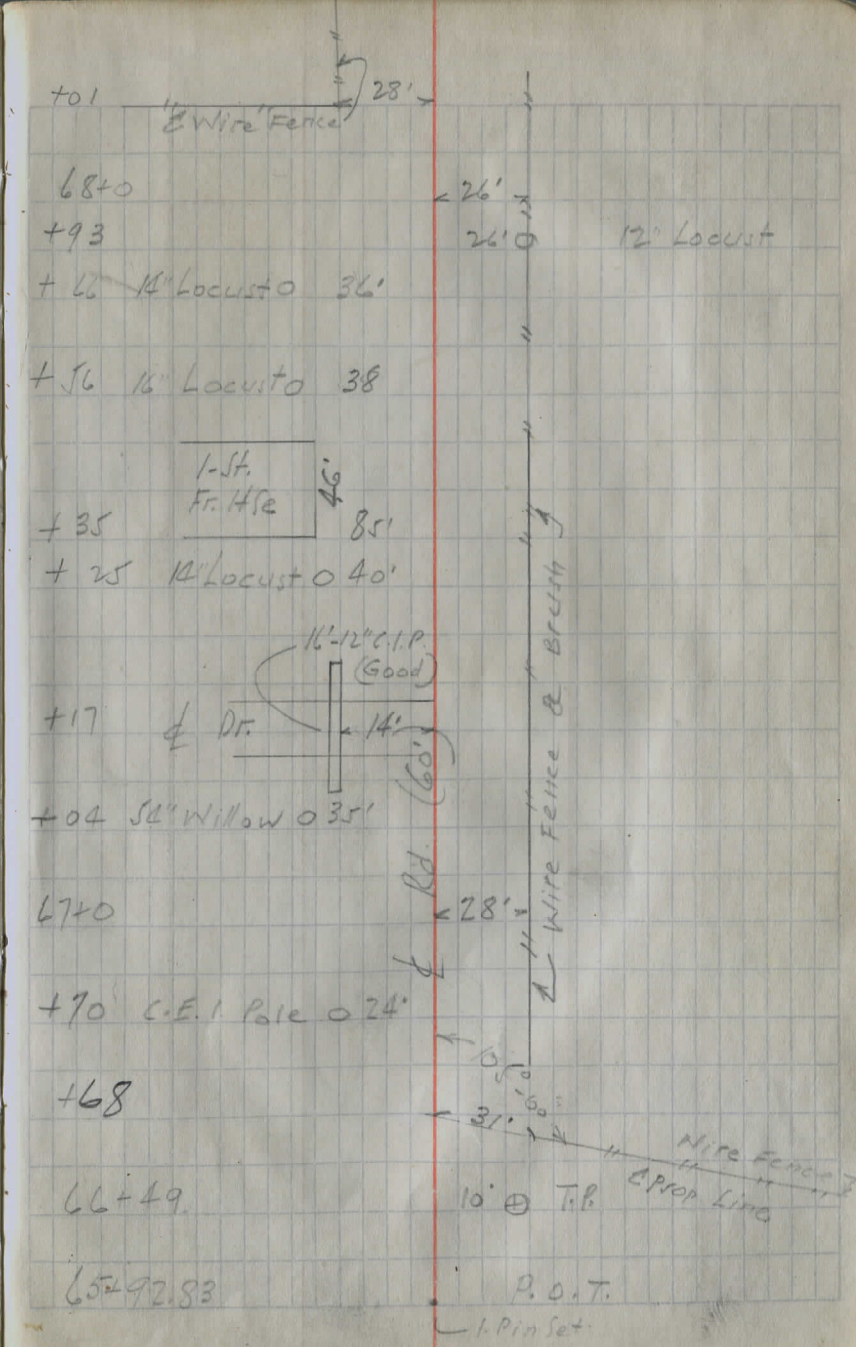
60+0

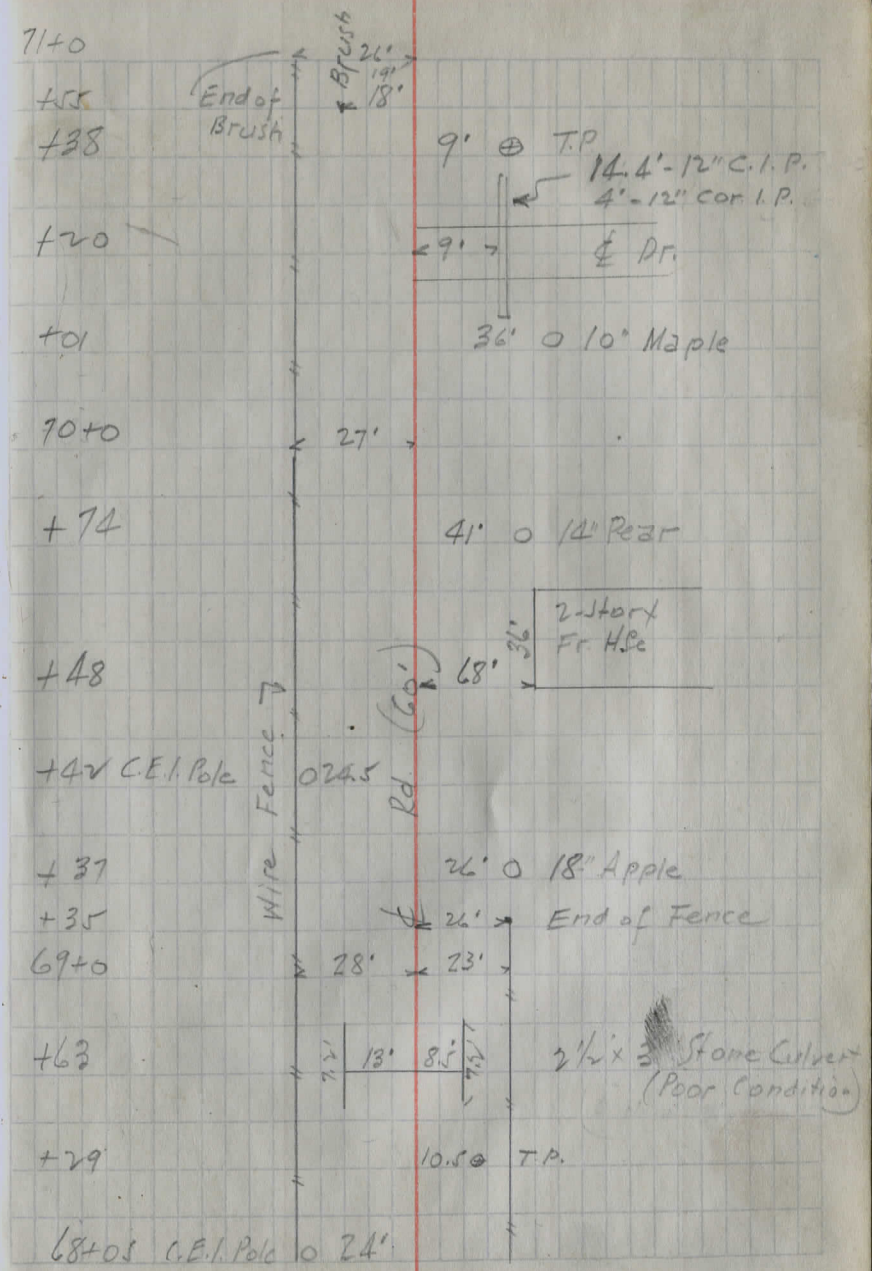


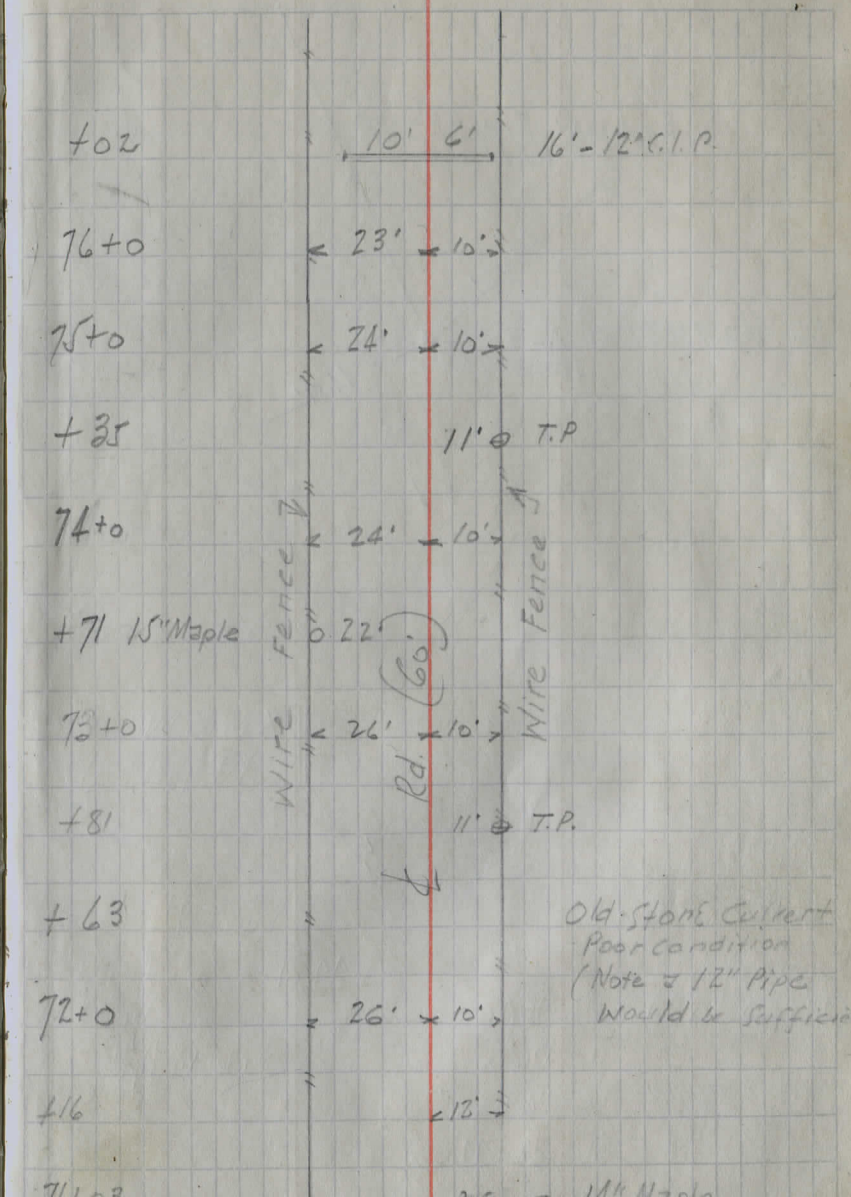
60+10.33 P.O.T.

OK Apr '39

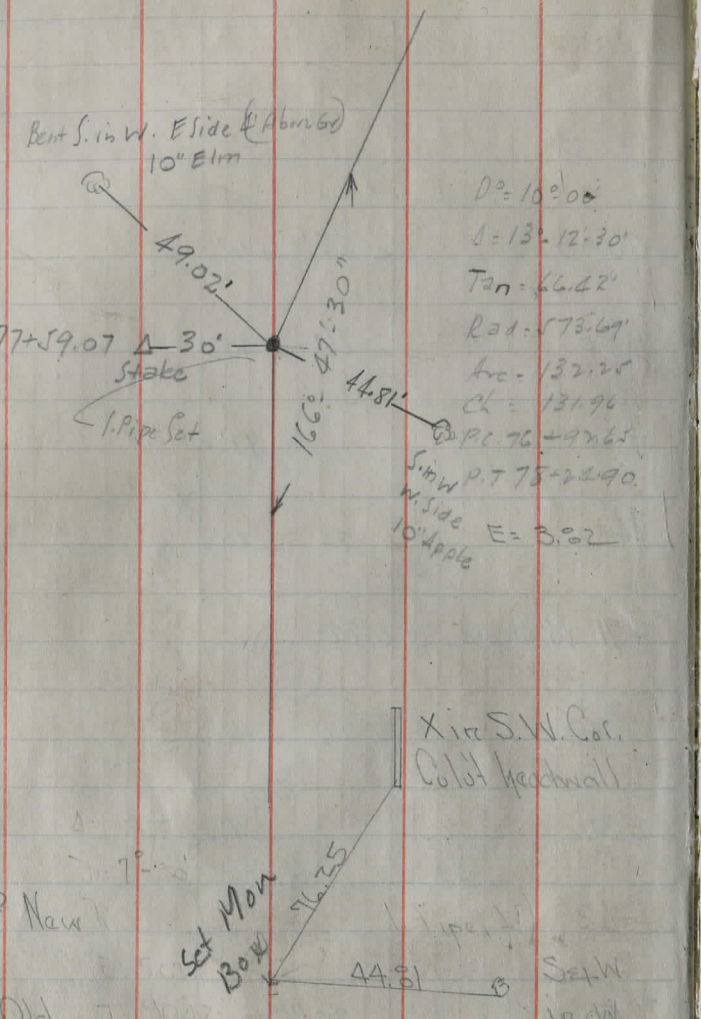



+01
28'
2 Wire Fence
68+0
26'
26'
12" Locust
+93
+66 14" Locust 0 36'
+56 16" Locust 0 38
1-St. Fr. Hse
46'
85'
+35
+25 14" Locust 0 40'
16"-12" C.I.P. (Good)
+17 ℄ Dr.
14'
+04 56" Willow 0 35'
(60')
℄ Rd.
67+0
28'
Wire Fence & Brush
+70 C.E.I. Pole 0 24'
+68
31'
Wire Fence
℄ Prop. Line
66+49
10' ⊕ T.P.
65+92.83
P.O.T.
1. Pin Set
65+92.83
1. Pin Set


71+0
+55
+38
+20
+01
70+0
+74
+48
+42 C.E.I. Pole
+37
+35
69+0
+63
+29
68+05 C.E.I. Pole
End of Brush
Brush
26'
19'
18'
9' ⊕ T.P.
14.4'-12" C.I.P.
4'-12" Cor I.P.
9'
℄ Dr.
36' ○ 10" Maple
27'
41' ○ 14" Rear
2-Story Fr. Hse
34'
68'
Wire Fence
Rd. (60')
024.5
26' ○ 18" Apple
26'
End of Fence
28'
23'
2'
13'
8.5'
4.5'
2½' x 3' Stone Culvert
(Poor Condition)
10.5 ⊕ T.P.
○ 24"

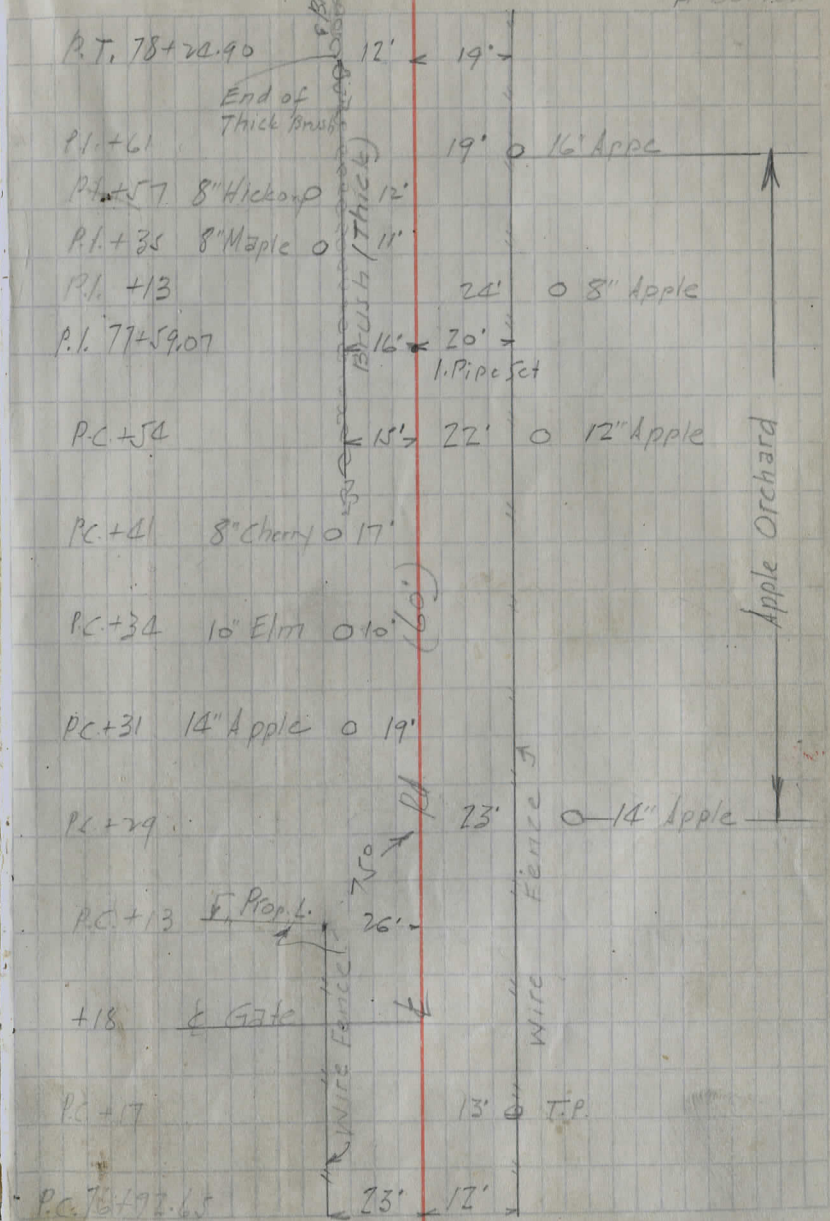

+02
10'
6'
16'-12" C.I.P.
76+0
23'
10'
75+0
24'
10'
+35
11'
T.P.
74+0
24'
10'
+71 15" Maple
22'
73+0
26'
10'
+81
11'
T.P.
+63
72+0
26'
10'
+16
13'
71+03
25
14" Maple
Wire Fence
Wire Fence
Rd. (60')
Old Stone Culvert
Poor Condition
(Note 2 12" Pipe
Would be Sufficient)

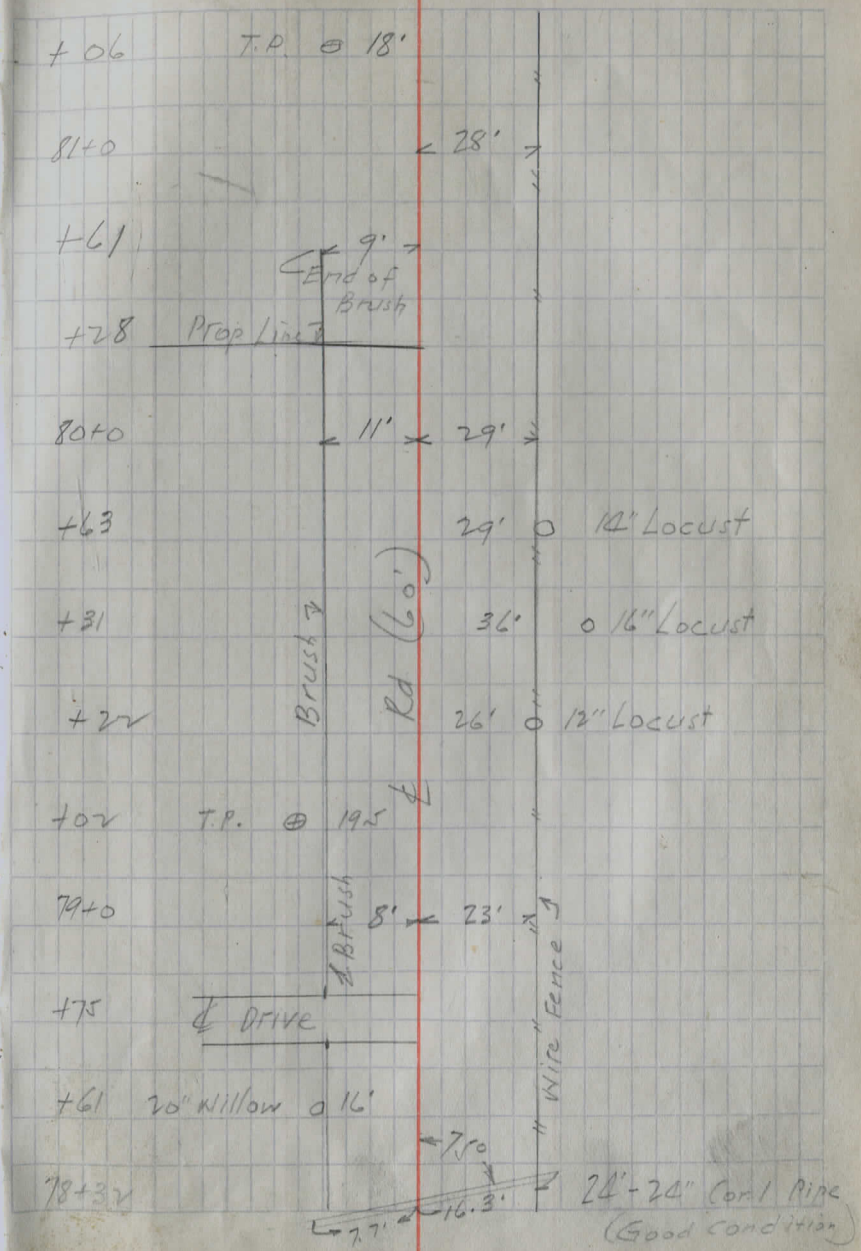
Wilsons Mills Rd

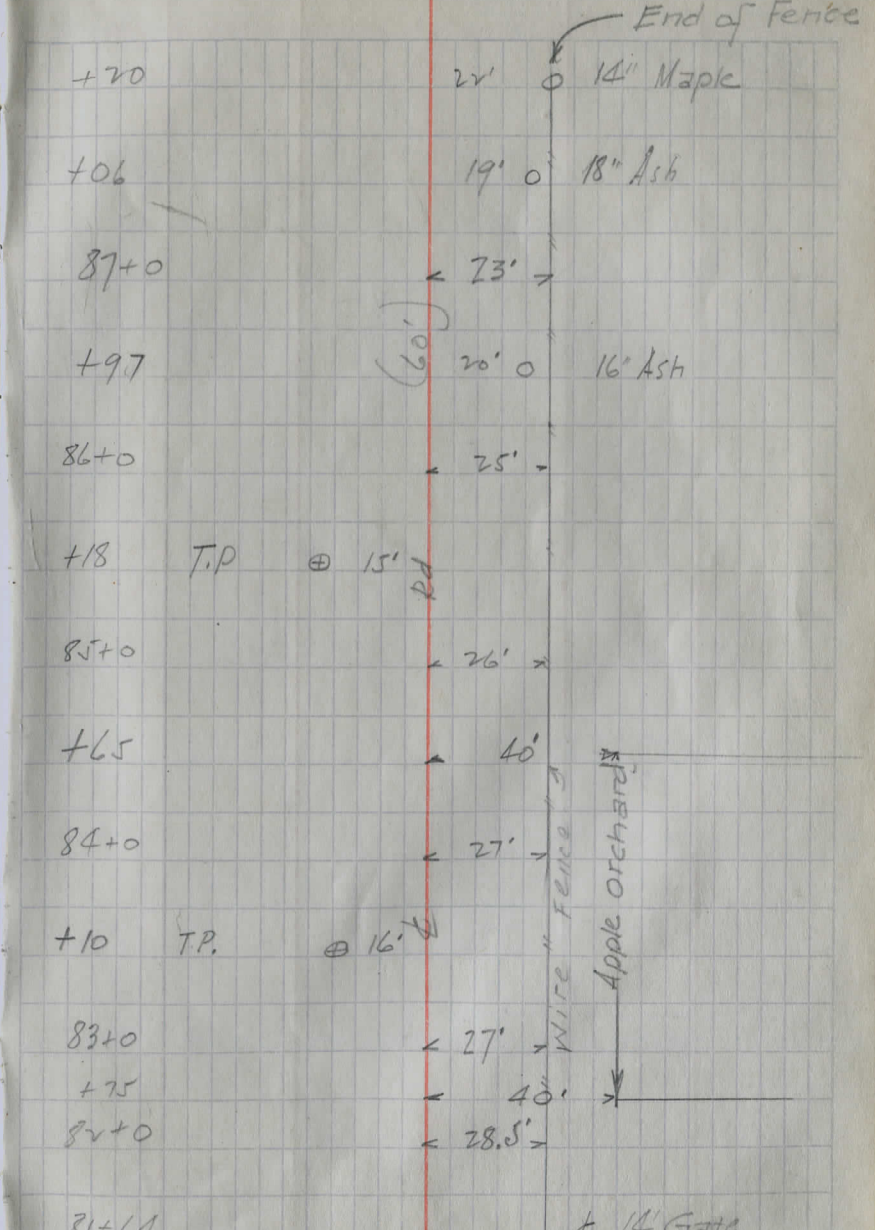


April 29, 1930 (Fair)

S Gold Jr
S Merritt
H Barton




+06
T.P. ⊙ 18'
81+0
28'
+61
9'
End of Brush
+28
Prop Line
80+0
11'
29'
+63
29'
12" Locust
+31
36'
16" Locust
+27
Brush
Rd (60')
26'
12" Locust
+02
T.P. ⊙ 19
79+0
8'
23'
Brush
+75
℄ Drive
+61
20" Willow ⊙ 16'
Wire Fence
78+32
7.0
16.3'
7.7'
24"+24" Corl Pine
(Good condition)


End of Fence
+20
2r'
14" Maple
+06
19'
18" Ash
87+0
23'
(20')
+9.7
20'
16" Ash
86+0
25'
+18
T.P
15'
85+0
26'
+65
40'
84+0
27'
+10
T.P.
16'
Wire Fence
Apple orchard
83+0
27'
+75
40'
82+0
28.5'
81+65
℄ 14' Gate

+65 ←1/200 Prop Line

+64 33' ○ 20" Maple

90+31 23' ○ 15" Maple

+98 23' ○ 16" Maple

+64 23' ○ 14" Maple

+31 23' ○ 18" Maple

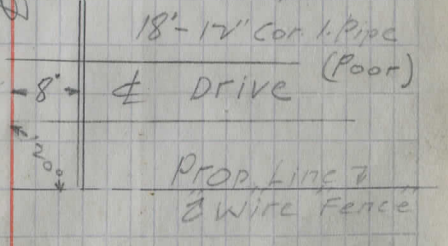
89+15 T.P. ⊕ 13'

+98 (60') 22' ○ 18" Maple

88+64 Rd. 22' ○ 18" Maple

+95 22' ○ 14" Maple

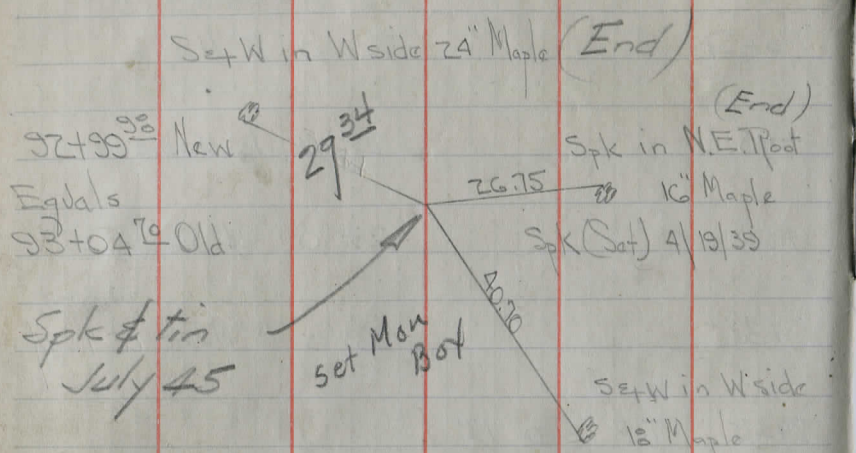
+61 23' ○ 18" Maple



+40

+34

87+73 T.P. ⊕ 14'

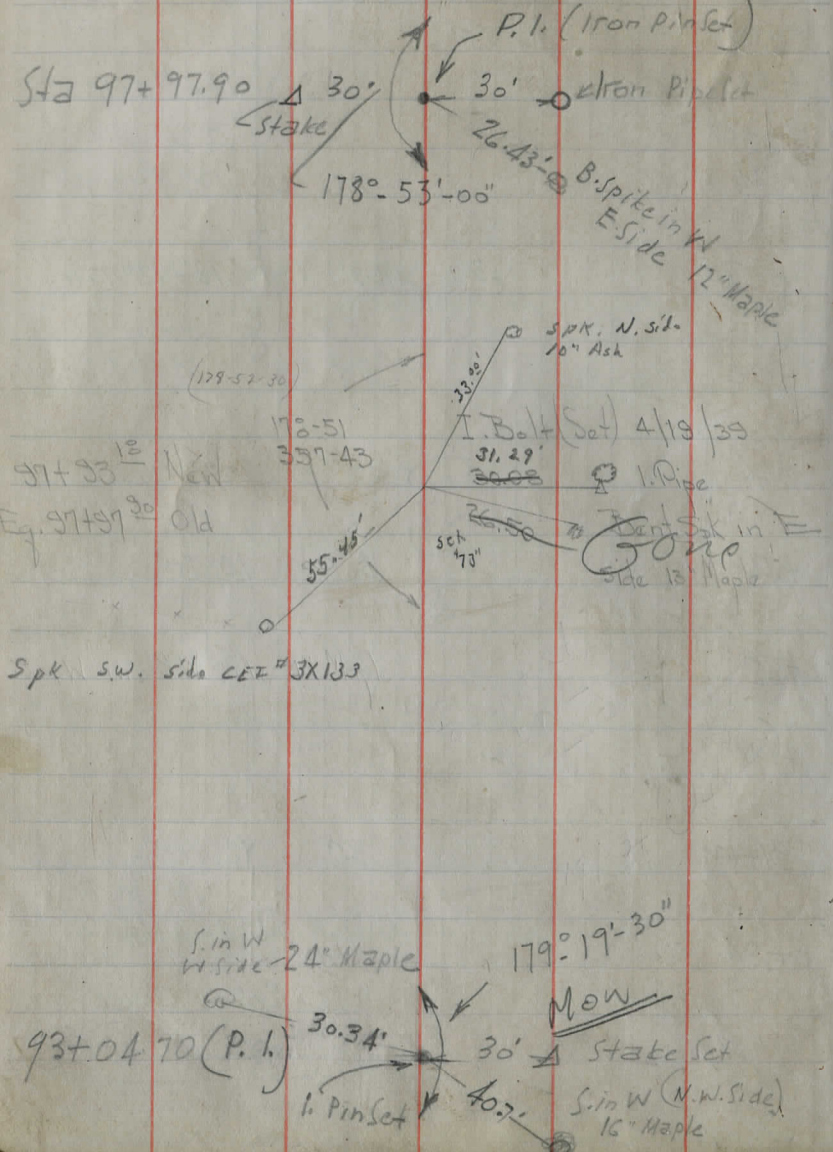


93+03 22" Maple ○ 26'
+93
+74
+62 10" Apple 1½-St. Fr. Hse 35' ○ 18'
+50 55'
+41
92+08
+76
+75 3.7' 14.3'
+70
+64
+56
+38
+19 T.P. ⊕ 12'
91+12
+84
90+83

41' ○ 18" Apple
27' ○ 16" Maple
26' ○ 18" Maple
26' ○ 18" Maple
25' ○ 12" Stump
18"-12" Tile
30' ○ 14" Willow
32' ○ 20" Willow
30' ○ 10" Tree
24' ○ 14" Maple
35 ○ 18" Maple
1½-St Fr House
45'
120'
20'-12" Cor. I. Pipe (Rear)
13' ± Dr.

Orchard
℄ Rd (60')

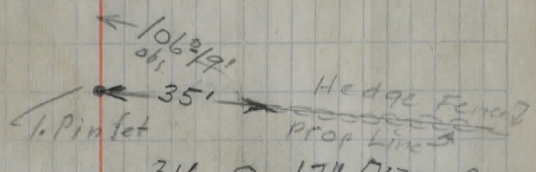
Wilsons Mills Rd (60')



April 30, 1930 (Fair)

J. Gold Jr.
J. Merritt
H. Barton

99+74 T.P. ⊕ 12'



+91 31' ○ 12" Osage Orange

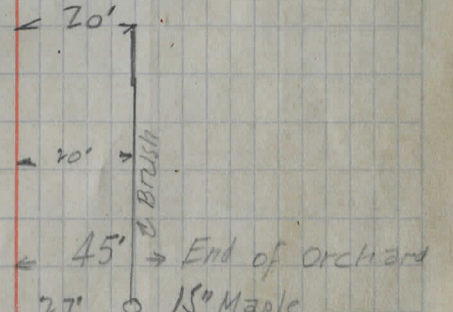
+89 25' ○ 12" Maple

+37 T.P. ⊕ 14.5

97+35 Prop L. & Wire Fence 25'
106°-30'

95+39 T.P. ⊕ 13.5'

+85



+57 T.P. ⊕ 12'

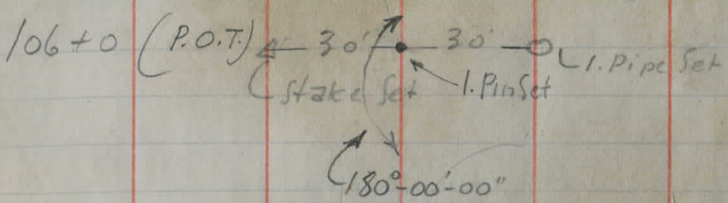
+15 24" Maple ○ 27'

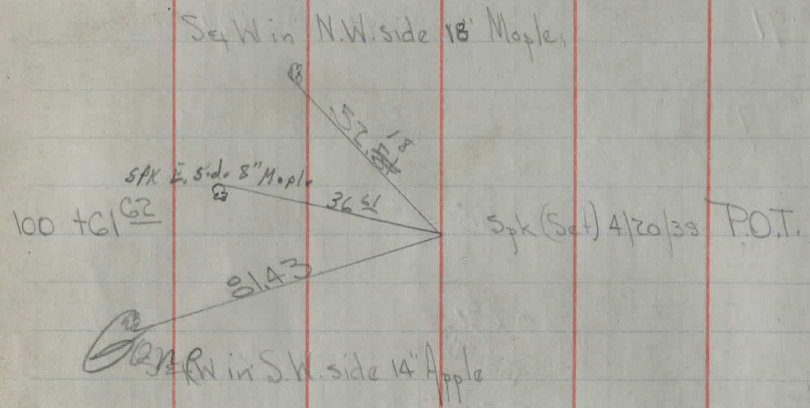
+10

+07

93+04.70 (P.I.) Iron Pin Set

Wilsons Mills Rd. (60')

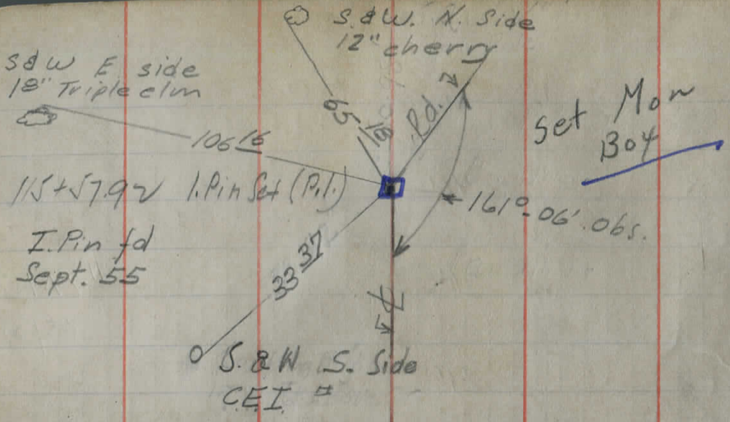




106+0	21'	P.O.T. 1. Pin Set
+64	T.P. ⊕ 11'	
105+0	21'	
104+0	21'	
+68	T.P. ⊕ 9'	
103+00	19'	
+05	19'	
102+02	T.P. ⊕ 10'	
+86	8" Cherry ○ 28'	
+62	℄ Dr.	
+34	8" Maple ○ 30'	
101+08	10" Maple ○ 30'	
100+89	1½-St. Fr. Hse 44'	69'

Hedge

Rd (60')



See page 33

115+49.71 New
Equals
115+57.92 Old

I. Pin (fd)

Δ = 18°-55' Rt
D = 8°-00'
R = 716.20
T = 119.44
E = 9.97
L = 236.46
P.C. = 114+30.27
P.T. = 116+66.73

4/20/39

Pomeroy
Fisher
Willman

161°-06' obs.

+57.92 ℄ N. & S. Rd. ℄ Fowlers Mills Rd
I. Pin Set

+24 T.P. ⊕ 15'

115+0

107°-53' obs. 28'

114+0 Brush

+85 9.5" 11.0' 4' x 1.5' H'd Walls

112+83 T.P. ⊕ 14' 14' (18" x 6" Stone Culvert)

110+22 T.P. ⊕ 12'

+37 33' ○ 16" Hickory

+35 30' ○ 18" Hickory

18' - 12" Cor. I. Pipe (Poor Cond.)

109+17 6' ℄ Dr.

112-St Fr. Hse

+41 50' 40'

+18 24' ○ 20" Maple

108+03 20' ○ 16" Willow

+86 T.P. ⊕ 17'

107+67 20' ○ 18" Willow

106+13 * 21'

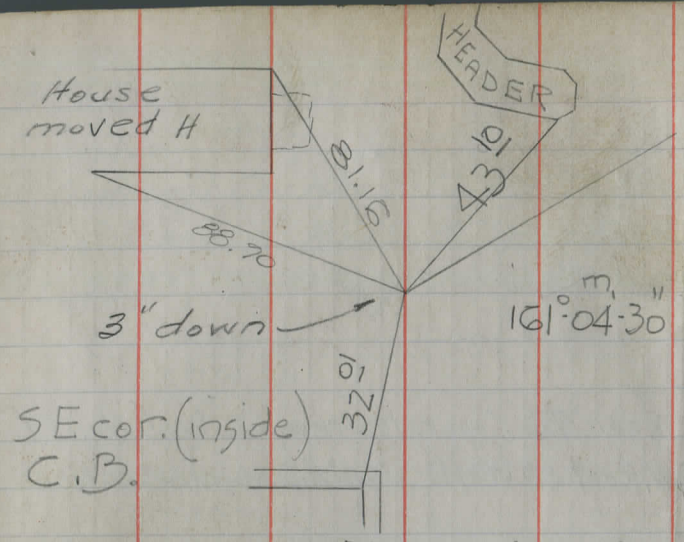
End of Hedge

WILSON MILLS ROAD.

Munson Twp. from Bloody Corners to Downing's Corners. Co. Hwy #8, Sec. H.
Road Record Book C, page 242.
Dec., 1835, Statutory width 60 feet.

		℄ C.H. 8+7.H. 108	
B.M.	Bloody Corners		1253.96
B.M.	Downing Corners	℄ C.H. 498	1311.43

Nail in N.W. cor., Top Concrete Step, School House.
Spike S.W. Root 30" Maple, 160' N.E. of intersection.



Spls set at 147.78 E & W (P.C. & P.T.)

Note. See page 31 for Curve data.

Sta 0+00 Beginning of Project

OFFSET STAKES, 25th Right, Sta. 1 to 29, inc.

Apr. 19, 1938, Fair, Windy, 70°±

W. C. Marks
Elmer Richards,
Harry H. Fowler.

24.5 12" Locust 7+60

7+18 C.E.1.193906X 26

7.0 8.7 6+51, 12" Cast Iron Pipe

5+69 C.E.1.193907X 25

4+19 C.E.1.193908X 26

2+95 .193909X 26

Embankment

C.E.1. 193910X 1+70 26

1+47 = 1+21

120'± School House 0+74

0+78 Tel. pole #140 23

R.P.s Foundation Corners

10" Cherry 0+60 23

0+62 House (moved) 0+37

6.1' 5.0 S

18.7 33.9 0+36 15" Vit. Pipe

8.1.16

88.90

89°03' 96.00

161°06' .90

Normalk

Fowlers Mills

Mon Box

5.80

20" Locust

Road.

N

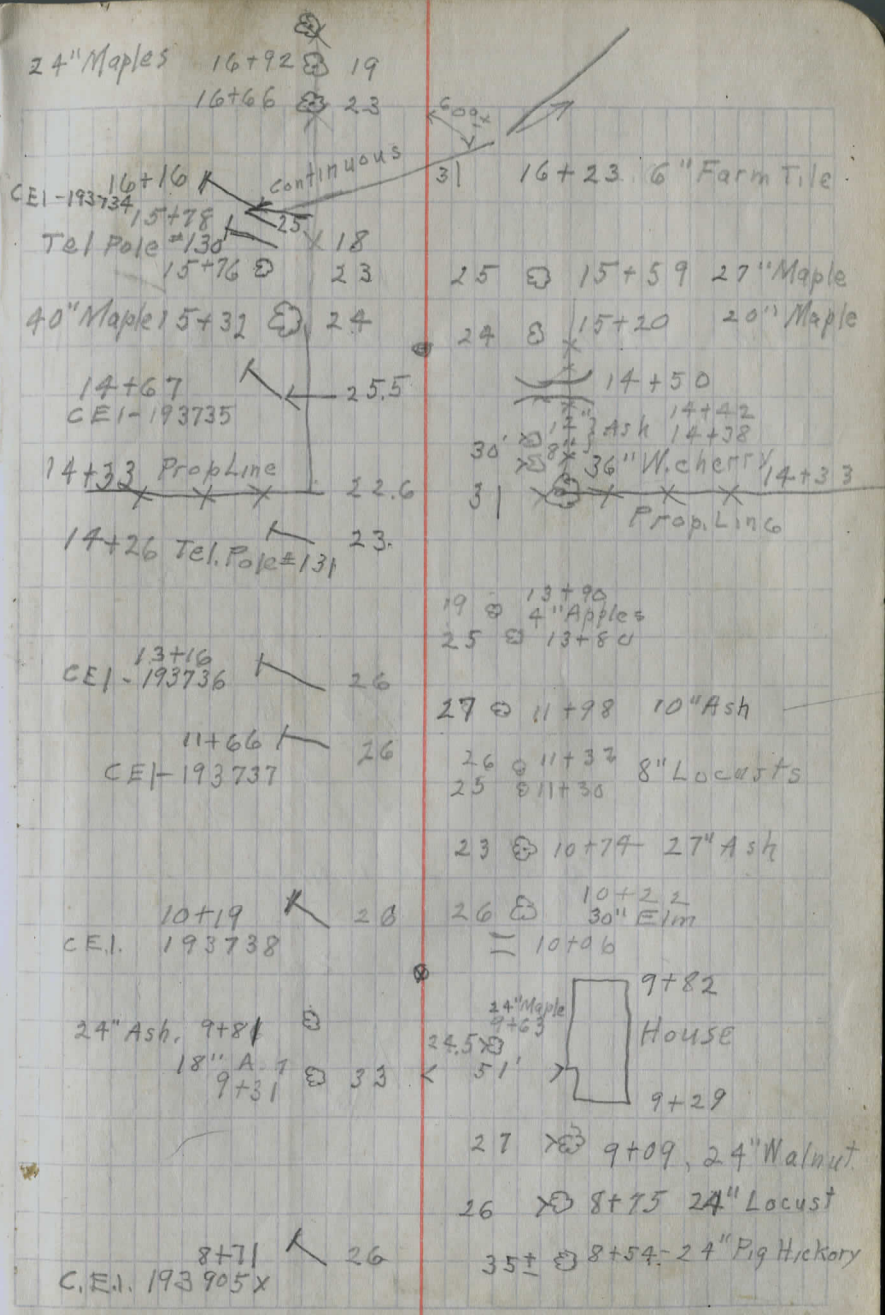
97+97.90 from tree reference only

Apr. 20, 1938, Cloudy, 60°±
W.C. Marks, Elmer Richards
H.H. Fowler,

15+00 P.O.T. Spike set on ℄

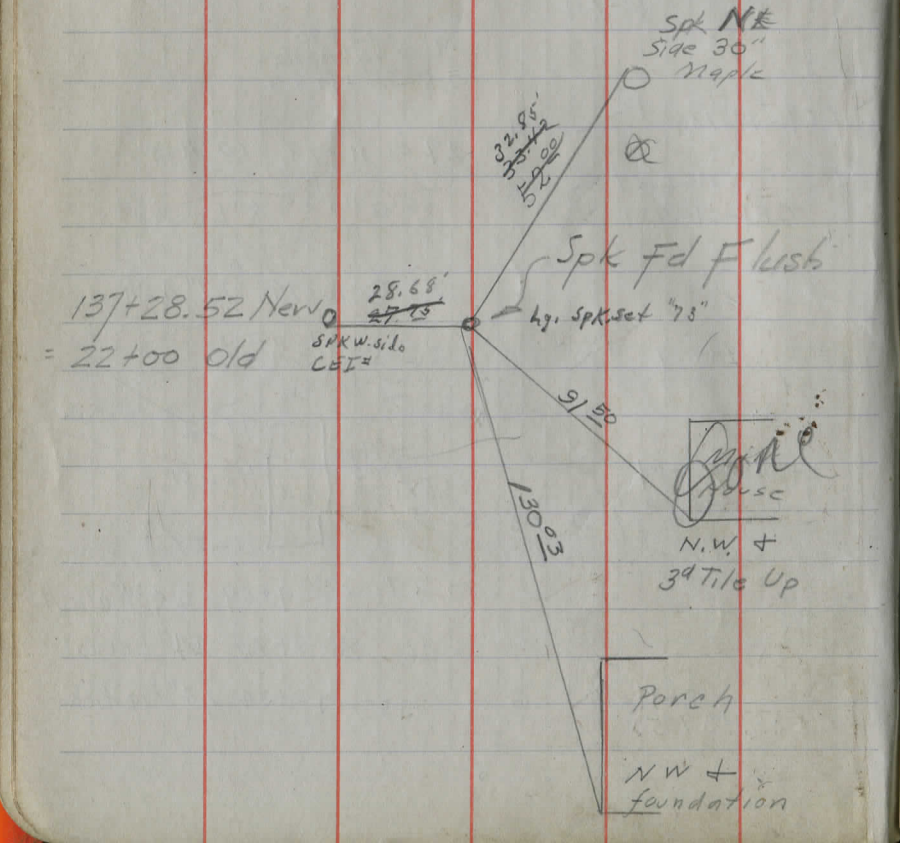
Stopped, Apr. 19, 1938

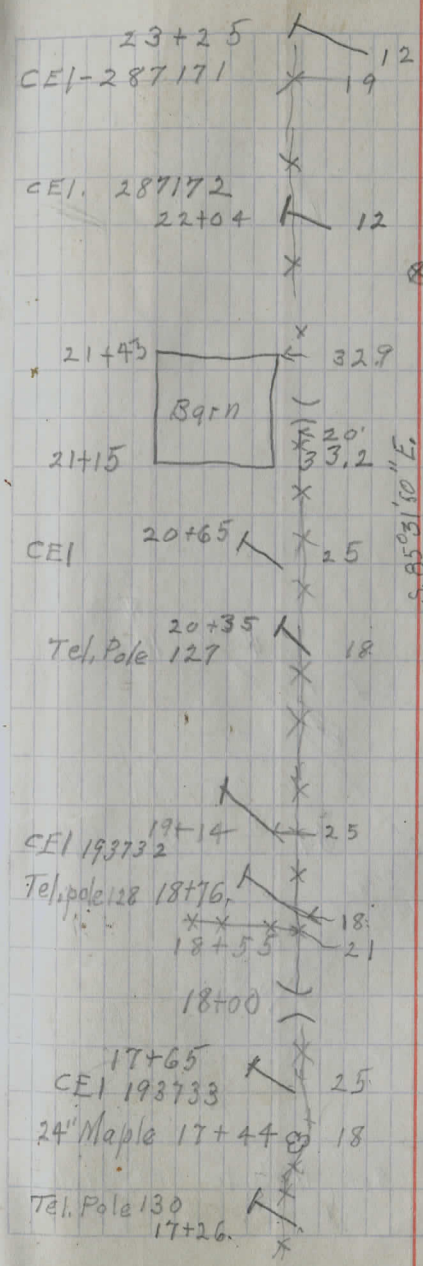
10+00 P.O.T. Spike set on ℄.

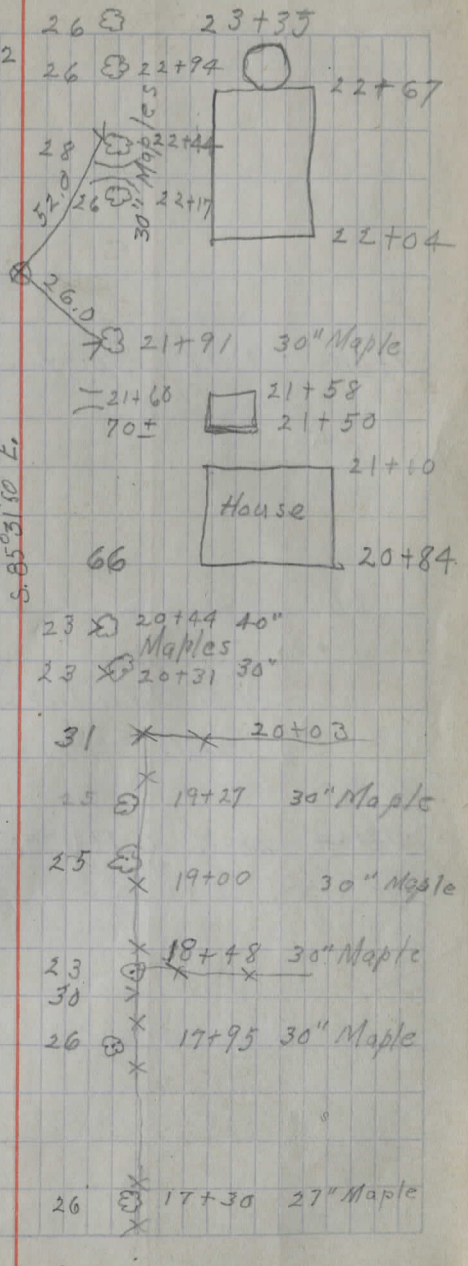


22+00 P.O.T. Lag Screw set on ℄

137+48 22

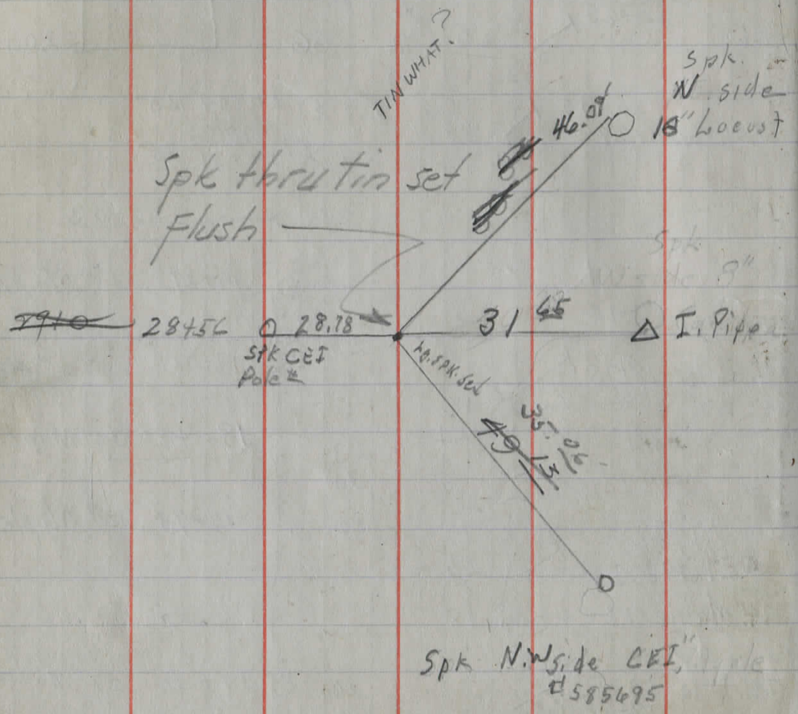






29+00 P.O.T. spike

144 +40 43



32+98 CEI- 287163 15

20 32+68 15" Apple

31+78 CEI-287164 14.7

31+50 CEI- 287165 14.4

30+00 Stake 25'

29+48

29+33 CEI 287166 14

40.31 8" Catalpa

25' Catalpa Grove

49.23

24 28+56 R.P. N.E. Root 30" Maple

24 28+26 30" Maple

28+14 CEI- 287167 13.5

6" Apples

23 27+60 36" Maple

22 27+49 24" Maple

26+90 CEI-287168 13

1st Row

Orchard

Iron Pipe fd.

26

26+17 Property Line 17.5

28.1

26 26+06 20" Elm

25+67 CEI. 287169 13

26 25+38 30" Maple

21.5 25+20 24" Maple

27 24+95 30" Maple

22 24+63 30" Maple

24+43 CEI 287170 12.5

23.5 23+98 30" Maple

27.5 23+49

stopped, Apr. 20, 1938

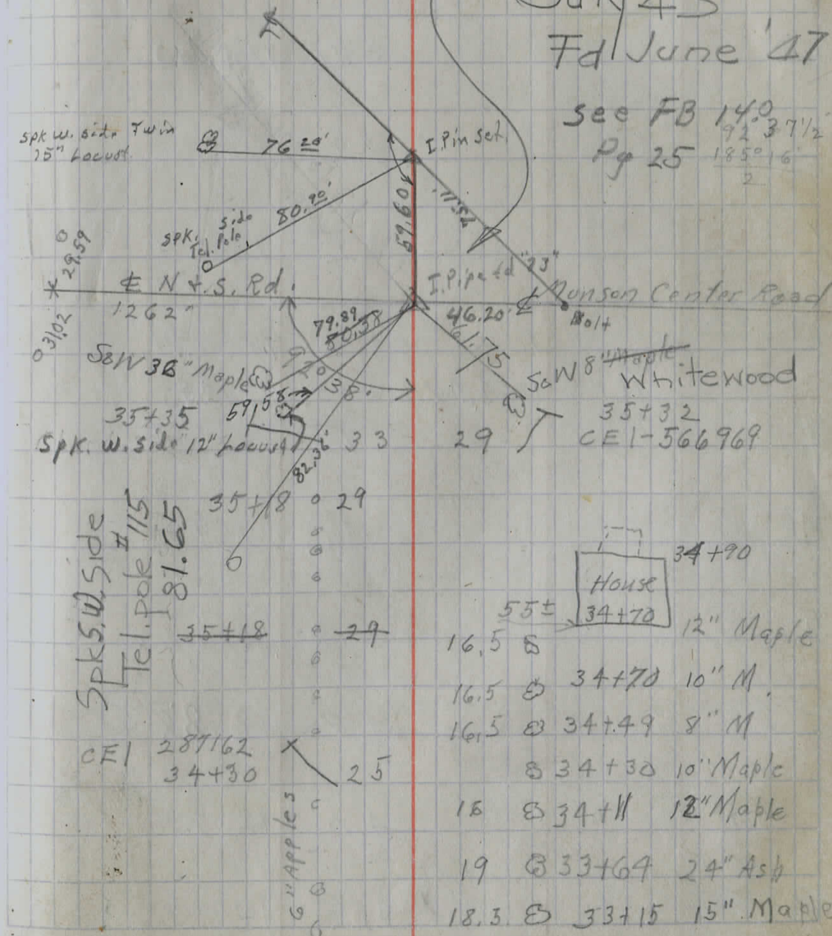
36+10.15 Bolt, found + used, ℄ N.+S. Center Rd.
151+58.02

± 89+73 Corp line to bolt at Downngs XS June '47

Bolt FD & reset Flush

July 45
Fd June '47

see FB 140 Pg 25
92 37½
185° 16
2



	1.40	1254.46		1253.06
0-300			6.9	1247.6
0-200			7.2	1247.3
0-100			6.7	1247.8
0+00			4.5	1250.00
B.M			3.86	1250.60
0+36			3.9	1250.50
1			3.2	1251.26
2			2.2	1252.26
	11.05	1263.48	2.03	1252.43
3			9.9	1253.58
4			8.6	1254.9
5			6.7	1256.8
6			4.7	1258.8
6+51			4.0	1259.5
7			3.2	1260.3

5.0 / 30

Gould's Elevation (1253.96[5])

B.M., N.W. Cor. Top concrete step, School House

Road N. 3.8/300 3.8/200 3.6/100 3.7/30 4.5/0 5.4/50 5.8/100 6.9/200 8.1/300 Road S.

N.E. Cor., North Headwall, 0+36

2.7/27 F.L. 6.5 3.9/18.7 4.4/17.7 3.9/0 4.6/32.9 4.1 7.0/33.9 F.L. 7.1/55

2.6/30 2.9/18 4.8/14 4.0/12 3.2/0 3.8/16 5.0/20 3.8/25 3.4/30

1.0/30 1.0/18 3.4/13 2.7/11 2.2/0 2.5/12 3.4/14 2.5/16 3.0/30

9.2/30 9.0/18 11.4/13 10.4/11 9.9/0 9.9 10.9/14 9.9/16 10.2/30

7.6/30 7.3/19 10.3/12 9.4/10 8.6/0 9.2/13 9.5/15 8.5/17 8.6/30

4.9/30 5.1/19 8.1/11 7.1/9 6.7/0 7.1/12 7.6/14 6.9/16 7.1/30

5.2/30 5.0/13 6.0/11 5.1/9 4.7/0 5.1/11 5.8/16 6.5/30

4.1 5.8/15 11 F.L. 6.4 4.1/7.0 4.0/0 4.5 6.4/8.7 F.L. 6.7/25 7.4/50 9.6/150

4.4/30 5.0/22 4.5/21 3.5/13 4.4/11 3.7/8 3.2/0 3.8/11 5.0/14 4.5/15 5.2/30

		1263.48		
8			1.4	1262.1
	12.87	1275.13	1.22	1262.26
9			10.1	1265.0
10			5.7	1269.4
11			1.9	1273.2
B.M. set.			4.66	1270.47
	12.16	1282.63		1270.47
12			6.2	1276.43
	12.99	1293.18	2.44	1280.19
13			12.4	1280.8
14			7.2	1286.00
14+75			3.5	1289.7
15			3.3	1289.9
15+65			5.7	1287.5
16			6.7	1286.5
16+15				
16+33				

1.4/30 1.7/23 2.1/20 1.4/15 2.6/11 2.0/9 1.4/6 — 1.7/10 2.2/13 1.7/14 1.9/30

Top of Stake 8+00

9.6/30 9.8/20 9.5/14 11.0/11 10.6/9 10.1/0 — 10.3/10 10.7/12 8.3/17 8.2/30

5.4/30 5.1/13 6.5/10 6.2/9 5.7/0 — 5.9/11 6.6/12 4.5/16 4.6/30

2.2/30 2.2/19 1.7/12 2.7/10 2.1/9 1.9/0 — 2.4/12 3.1/13 1.8/15 1.6/30

Spike, N.W. Root, 24" Maple 24' Right 9+63

Apr. 23, 1938

4.6/30 5.0/13 6.5/9 6.2/0 — 6.5/11 7.0/14 4.6/17 3.8/30

9.6/30 9.9/12 12.9/8 12.4/0 — 12.6/11 12.8/14 10.5/18 9.5/30

5.0/30 5.0/13 7.7/9 7.2/0 — 7.4/11 4.8/15 4.6/30

2.9/30 2.3/13 4.2/11 3.9/10 3.3/0 — 4.0/12 1.8/16 1.1/30

5.5/30 5.6/15 7.1/11 6.0/8 5.7/0 — 6.4/11 4.6/14 3.2/30

9.0/30 9.0/13 7.0/8 6.7/0 — 7.2/11 7.9/18 10.0/30

11.8/19 F.L. 6" Tile, Continuous from Field across Road

12.7/30 F.L. ~~6" Tile~~, 6" Tile Continuous

		1293.18		
16+33			6.8	1286.4
17			6.1	1287.1
18			4.1	1289.1
B.M. set.			7.20	1285.98
	12.55	1305.54	0.19	1292.99
19			11.9	1293.6
20			5.6	1299.9
	10.70	1316.19	0.05	1305.49
21			10.0	1306.2
21+50			7.0	1309.2
22			6.0	1310.2
23			5.5	1310.7
24			4.5	1311.7
25			2.9	1313.3
B.M. set			1.68	1314.51

~~#6~~

11.6 / 33 — 13.3 / 85 — 15.4 / 13.5 — Surface

3.4/30 — 4.7/19 — 6.6/13 — 7.3/11 — 6.4/8 — 6.1/0 — 6.5/11 — 7.5/15 — 9.8/30

3.7/30 — 4.3/19 — 4.9/10 — 4.5/8 — 4.1/0 — 4.6/15 — 4.0/30

N. root 27" Maple, 26' Right, 17+30

11.2/30 — 11.2/12 — 12.8/10 — 12.2/8 — 11.9/0 — 12.1/12 — 7.2/17 — 5.4/30

5.0/30 — 5.2/13 — 6.3/10 — 5.9/8 — 5.6/0 — 5.3/2 — 6.0/11 — 6.2/14 — 3.7/18 — 2.2/30

7.6/30 — 7.5/13 — 10.7/9 — 10.4/7 — 10.0/0 — 10.0/2 — 9.7/12 — 10.2/13 — 7.1/16 — 6.8/30

5.9/30 — 7.6/11 — 7.4/5 — 7.0/0 — 7.4/11 — 8.1/13 — 6.5/17 — 6.7/30

5.2/30 — 5.3/11 — 7.3/9 — 6.4/7 — 6.0/0 — 6.1/11 — 7.0/13 — 5.9/17 — 5.9/30

5.5/30 — 5.9/13 — 6.8/9 — 6.0/7 — 5.5/0 — 5.2/5 — 6.1/14 — 6.6/16 — 7.1/25 — 8.9/30 — 15.9/100

3.5/30 — 4.6/11 — 5.6/8 — 4.7/5 — 4.5/0 — 4.3/4 — 5.0/15 — 4.7/25 — 5.2/30

2.0/30 — 2.6/11 — 4.0/8 — 3.0/5 — 2.9/0 — 2.7/4 — 3.6/16 — 3.5/25 — 4.0/30

Spike, N.W. Root, 30" Maple, 26' Right, 25+38.

	10.50	1325.01		1314.51
26			9.8	1315.2
27			7.5	1317.5
28			4.3	1320.7
29			2.1	1322.9
	3.55	1326.52	2.04	1322.97
30			3.9	1322.6
31			4.4	1322.1
32			4.5	1322.0
33			4.6	1321.9
34			5.9	1320.6
	1.11	1319.72	7.91	1318.61
35			1.7	1318.0
36			4.5	1315.2
36+10			4.8	1314.9
36+50			7.0	1312.7
37			9.4	1310.3
B.M.			8.29	1311.43

8.8/30 9.6/10 10.7/8 10.0/6 9.8/0 9.6/4 10.3/13 9.6/16 9.5/25 9.3/30

5.8/30 6.7/13 8.6/9 7.8/7 7.5/0 7.3/4 7.9/13 6.7/16 6.3/30

3.5/30 3.1/24 4.3/12 5.7/9 4.9/7 4.3/0 4.1/4 5.0/13 4.0/16 3.9/30

2.3/30 2.7/17 3.5/10 3.1/8 2.1/0 2.4/12 3.5/15 2.6/18 2.7/30

4.3/30-25 5.1/16 5.4/11 4.7/8 3.9/0 4.3/12 5.7/16 4.8/18 4.6/30

5.1/30 5.2/25 5.5/14 5.0/8 4.4/0 5.0/12 6.1/15 5.5/17 5.7/30

4.8/32 5.8/17 6.4/15 4.9/8 4.5/0 5.1/11 6.3/14 5.6/16 5.7/30

5.2/30 4.9/25 5.7/19 6.2/17 5.5/15 4.6/0 5.1/9 6.7/13 5.6/15 5.5/30

5.9/30-21 7.4/18 6.8/16 5.9/0 6.5/7 8.0/11 5.0/16 4.6/30

1.4/30 1.7/25 3.1/22 2.6/19 1.7/0 2.4/10 3.1/13 0.2/18 0.0/30

5.5/30 4.3/0 3.6/30

7.3/100 6.1/50 4.8/0 3.4/50 3.0/100

Spike SW root 30" Maple 160' NE of Sta 36+10

Check Levels

8.34	1319.77		1311.43
		1.15	1318.62
7.78	1326.40		
		3.45	1322.95
1.11	1324.06		
		9.56	1314.50
1.50	1316.00		
		10.50	1305.50
0.11	1305.61		
		12.60	1293.01
0.29	1293.30		
		~~1.00~~	
		13.00	1280.30
0.01	1280.31		
		9.84 ~~9.92~~	1270.47
0.30	1270.77		
		8.48	1262.29
0.99	1263.28		
		10.80	1252.48
2.00	1254.48		
		1.37	1253.11

B.M. S.W. root, Maple 160'± N.E. of Downing Cor.

~~7.31~~ 1

-7.31 | 1285.99 B.M

Different Point

Gould's survey, (1253.965)

N.W. Cor., Top (2nd) Concrete step., School House,

Check Levels

0.33	1256.27		1255.94
		2.40	1253.87

9.42	1294.86		1285.44
11.94	1306.59	0.21	1294.65
9.14	1315.39	0.34	1306.25
		3.89	1311.50

Spike, NE. Root Hickory, R. 109+25, (Goulds Survey)
N.W. cor., top, concrete step, (2nd), Sch. House, Bloody Corners

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B.M.#2, Downings Cor. N. Road.
Spike, E. root, 15" Maple. 25'L., Sta 9+90.

Spike, S.W. Root, Large Maple 160± N.E. of Downing's Cor.

8-4-38 + HI — Graber Dist 3 Richards Class

	+	HI	—		
BM#	6.21	1256.81			1250.60
0+00			5.62	1250.00	
1			5.55	1251.26	
2	6.72	1257.32	4.79	1252.53	1250.60
3			3.53	1253.79	
4			2.26	1255.06	
	8.59	1264.33	1.58		1255.74 TP
5			7.81	1256.52	
6			5.92	1258.41	
+51 culvert			4.83	1259.5± Gr. Rk.	
7			3.67	1260.66	
	9.21	1271.44	2.10	1262.23 TP	
8			0.95		BM 270.47
			8.11	1263.33	270.49
9			5.02	1266.42	
BM# 2	5.20	1271.67			1270.49
10			5.80	1269.87	
11			1.93	1273.74	
T.P.	9.24	1284.20	0.71	1274.96	
12			6.39	1277.81	

	Lt.	Rt.	
C 0.5 / 24.5	C 0.3 / 23.2	F 1.7 / 19.5	F 1.5 / 20.5
0.0 / 24.0	C 0.2 / 23.0	0.7 / 20.9	F 0.5 / 21.9
C 0.5 / 23.6	C 0.5 / 22.6	F.4 / 21.4	F 0.3 / 22.4
C 1.0 / 24.5	1.0 / 23.5	C.2 / 22.3	C 0.5 / 23.3
C 2.0 / 25.6	24.6	0.0 / 22.0	0.0 / 23.3
0.0 / 22.6	F 0.3 / 21.6	0.5 / 20.6	F 0.5 / 21.6
4.69 = El 125964 = ± Pave. + 51			
E 1.5 / 20.8	1.5 / 19.8	F 1.7 / 19.5	F 1.3 / 20.5
F 1.5 / 20.5	1.6 / 19.5	F 1.7 / 19.5	F 1.5 / 20.3
F 1.0 / 21.5	F 1.0 / 20.5	C 0.6 / 23.0	C 0.5 / 24.0
Gr. 0.0 / 22.4	C 4.0 / 21.4	C 1.0 / 22.9	C 1.0 / 23.9
F 1.0 / 21.4	F 1.1 / 20.4	Ea 1.0 / 21.9	Gr 0.0 / 22.9
Gr / 22.7	F 0.2 / 21.9	F 0.7 / 21.0	F 0.5 / 22.0

8-5-28

	+	H.I.	−	Elev.	
		1284.20			
13			2.32	1281.88	
T.P.	9.53	1293.49	0.24	1283.96	
14			7.55	1285.94	
15			4.81	1288.68	
+65					
16			4.69	1288.80	
			7.52	BM # 3 =	1285.98
					1285.97
17	7.03	1293.00	4.98	1288.02	
18			2.82	1290.18	
TP	1290	1305.61	0.29		1292.71
19			10.32	1295.29	
20			4.79	1300.82	
T.P.	9.85	1315.09	0.37		1305.24
21			8.87	1306.27	
+50.					
22			5.29	1309.80	
23			4.29	1310.80	
24			3.41	1311.68	
T.P.	8.24	1320.44	2.89		1312.20
25			7.01	1313.43	
BM#4			6.01		1314.51 BM
					1314.43

18 to 21 + 70 special

L

C 2.5	C 2.3	
26.4	25.4	
C 2.5	C 2.1	
26.0	25.1	
C 2.0	C 1.9	
25.8	24.8	
F 5.0	19.5 C 5.1	
25.2	24.2	
C 1.0	C 1.0	
24.5	23.5	
F 1.0	F 1.4	
20.9	19.9	
F 1.5	F 1.5	
20.8	19.8	
Gr 0.0	F 0.4	
22.4	21.4	
C 1.5	22	
26.3	25.3	
C 1.0	24.2 C 1.1	
24.6	23.6	
0.0	0.2	
22.7	21.7	
C 1.0	C 0.7	
22.0	21.0	
C 0.5	C 0.5	
23.7	22.7	

Rt.

C 1.9	C 1.0
23.5	24.5
C 2.9	C 3.0
26.3	26.3
C 3.2	C 3.5
26.8	27.8
19.8 F 5.8	F 6.0
25.6	26.6
F 3.6	F 3.5
20.8	21.8
F 1.4	F 1.4
20.0	21.0
C 4.2	C 4.5
26.5	27.5
C 1.5	C 1.5
21.8	22.8
C 3.0	C 3.0
24.0	25.0
21.5 C 0.6	C 1.0
22.9	23.9
F 1.6	F 1.5
19.6	20.6
F 0.4	0.0
21.4	22.4
F 0.8	F 0.5
20.8	21.8

8-8-38

	+	HI	−	EI	
		1320.44			
26			4.64	1315.80	
27			2.24	1318.20	
TP	7.49	1326.91	1.02		1319.42
28			6.31	1320.60	
29			4.15	1322.76	
30			4.13	1322.78	
T.P.	3.96	1327.19	3.68		1323.23
31			4.63	1322.56	
32			4.85	1322.34	
T.P.	3.10	1324.86	5.43		1321.76
33			2.89	1321.97	
34			4.36	1320.50	
35			6.96	1317.90	
36				1314.00	
T.P.	0.87	1318.06	7.67		1317.19
				BM =	1311.43
			6.69		1311.35

C 0.5 / 23.3 — C 0.2 / 22.3 — F 0.4 / 21.4 — 0.0 / 22.4

C 1.0 / 23.5 — C 0.6 / 22.9 — C 0.1 / 22.2 — C 0.5 / 23.2

C 1.0 / 24.0 — C 0.6 / 23.0 — C 0.2 / 22.3 — C 0.5 / 23.3

0.0 / 22.6 — F 0.3 / 21.6 — F 0.3 / 21.6 — 0.0 / 22.6

F 1.0 / 21.5 — E 1.0 / 20.5 — F 1.0 / 20.5 — E 1.0 / 21.5

= old BM 28+60

F 1.5 / 20.6 — F 1.6 / 19.6 — F 1.7 / 19.8 — F 1.5 / 20.5

F 1.6 / 20.7 — F 1.9 / 19.7 — F 1.5 / 19.7 — F 1.5 / 20.7

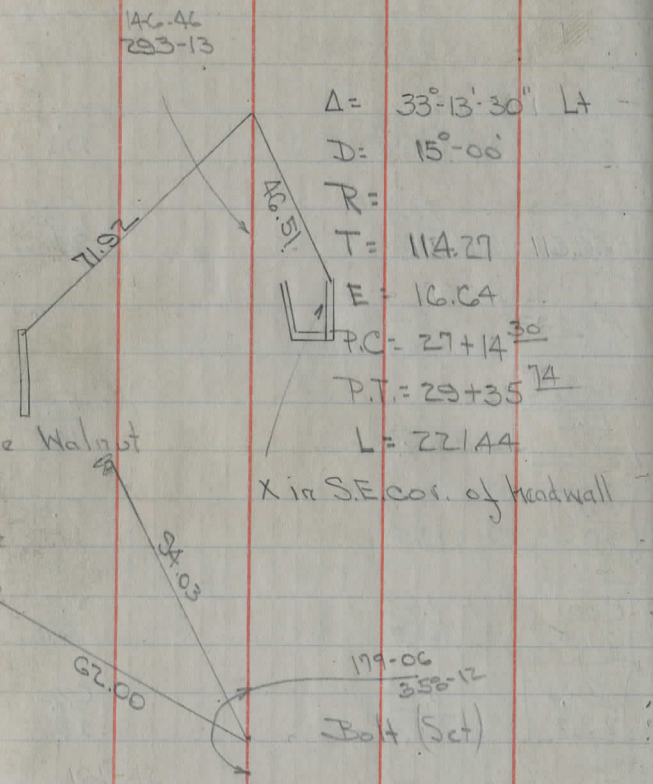
E 1.0 / 21.0 — F 1.3 / 20.0 — 1.1 / 20.4 — F 0.8 / 21.4

C 0.5 / 23.2 — 0.1 / 22.2 — C 1.2 / 23.8 — C 1.5 / 24.8

F 1.0 / 20.6 — F 0.9 / 20.6 — C 2.1 / 25.1 — C 2.5 / 26.1

21.8 — 22.0

Relocation Wilsons Mills Sta. 19+12.03 to

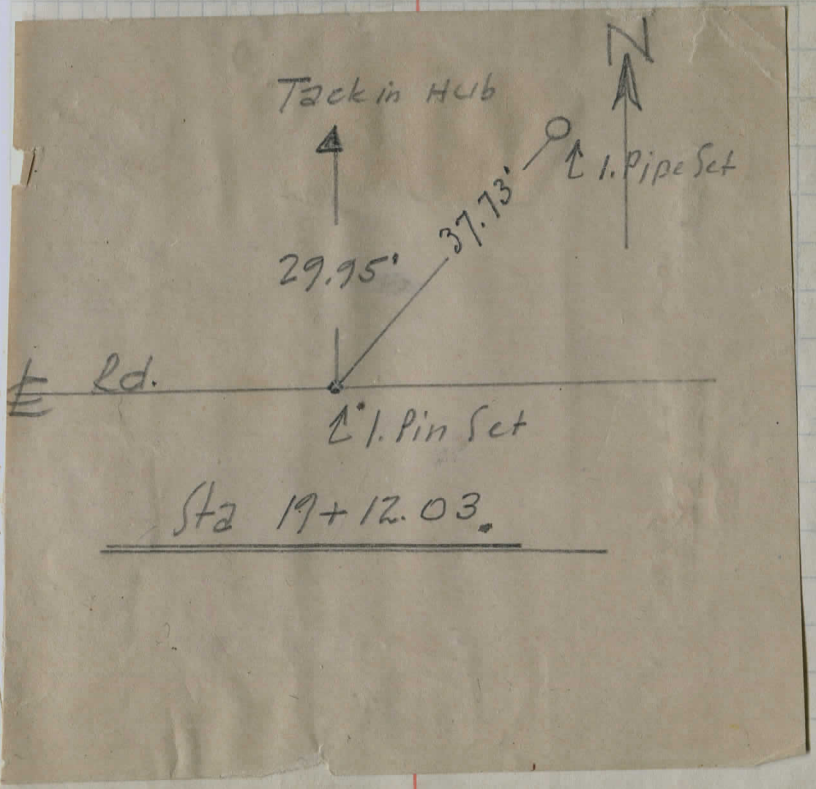


Δ = 33°-13'-30" Lt
D = 15°-00'
R =
T = 114.27
E = 16.64
P.C. = 27+14.30
P.T. = 29+35.74
L = 221.44
X in S.E. cor. of Headwall

Pomeroy April 1935
Fisher
Williman

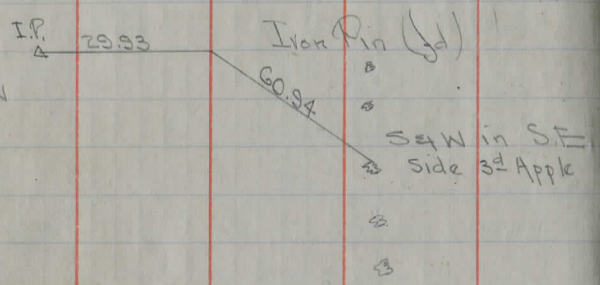
40

115.99



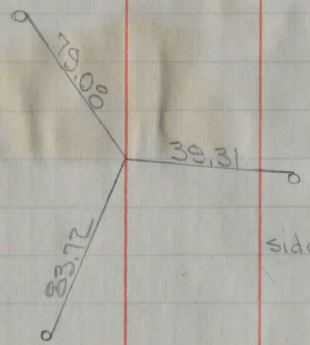
5080.75
4725.87
354.88

47+26 91 Old
Equals
47+25 87 New



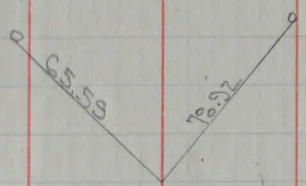
Spk&W in S. side T. Pole

36+23 92



S&W in S. side of T. Pole
S&W in N.W. side of T. Pole

37+46 45



I.Bolt(5/8d)

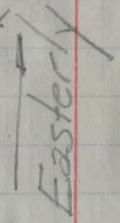
Δ = 27°-29 Rt
D = 15°-00'
T = 93.55
R = 383.05
E = 11.23
P.C. = 35+30.37
P.T. = 37+13.37
L = 183.00

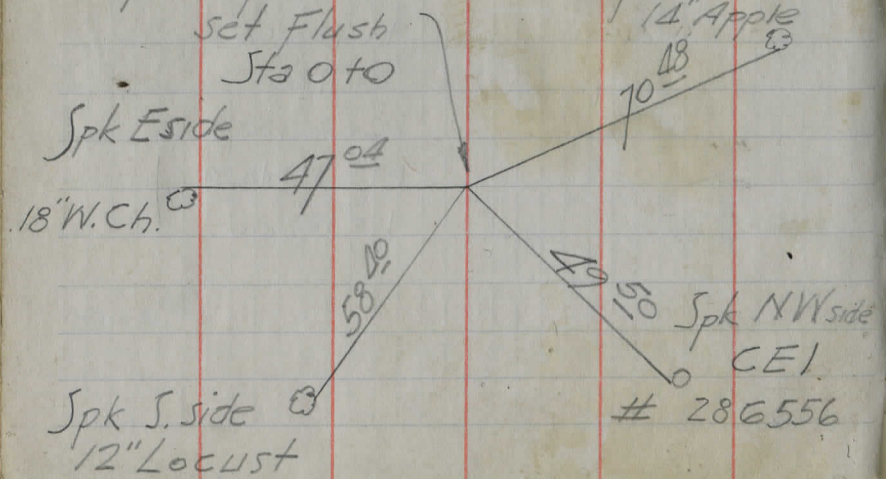
RETRACEMENT OF

July 1945 Pom-Canfield-Hall

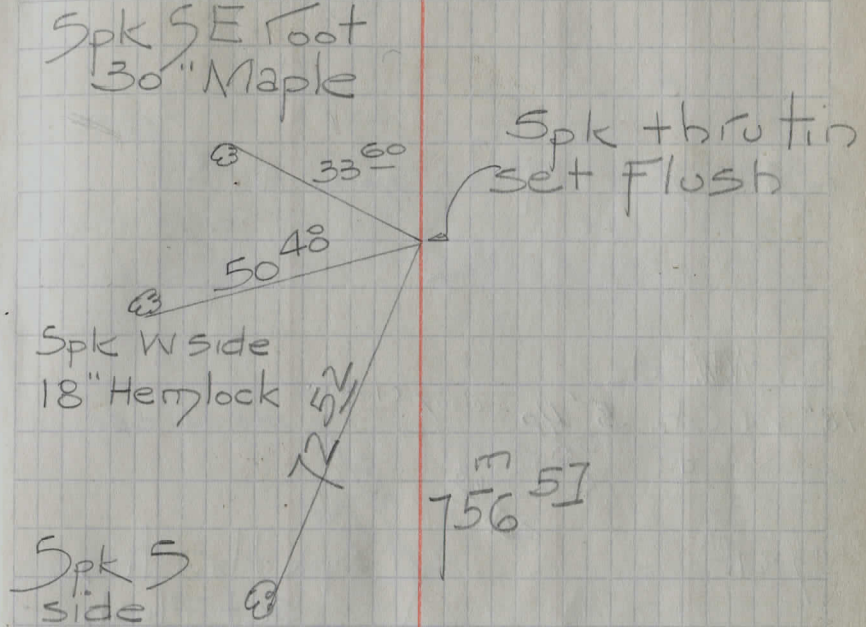
7+56.57 P.O.T

NOTE: Orig. survey (Apr. 1930) followed where same agrees approx. with travelled & otherwise new points set. See worksheet for plotting of both surveys

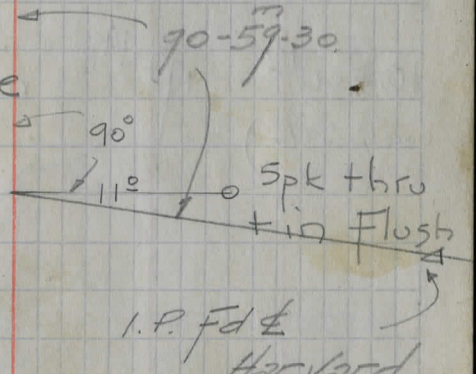


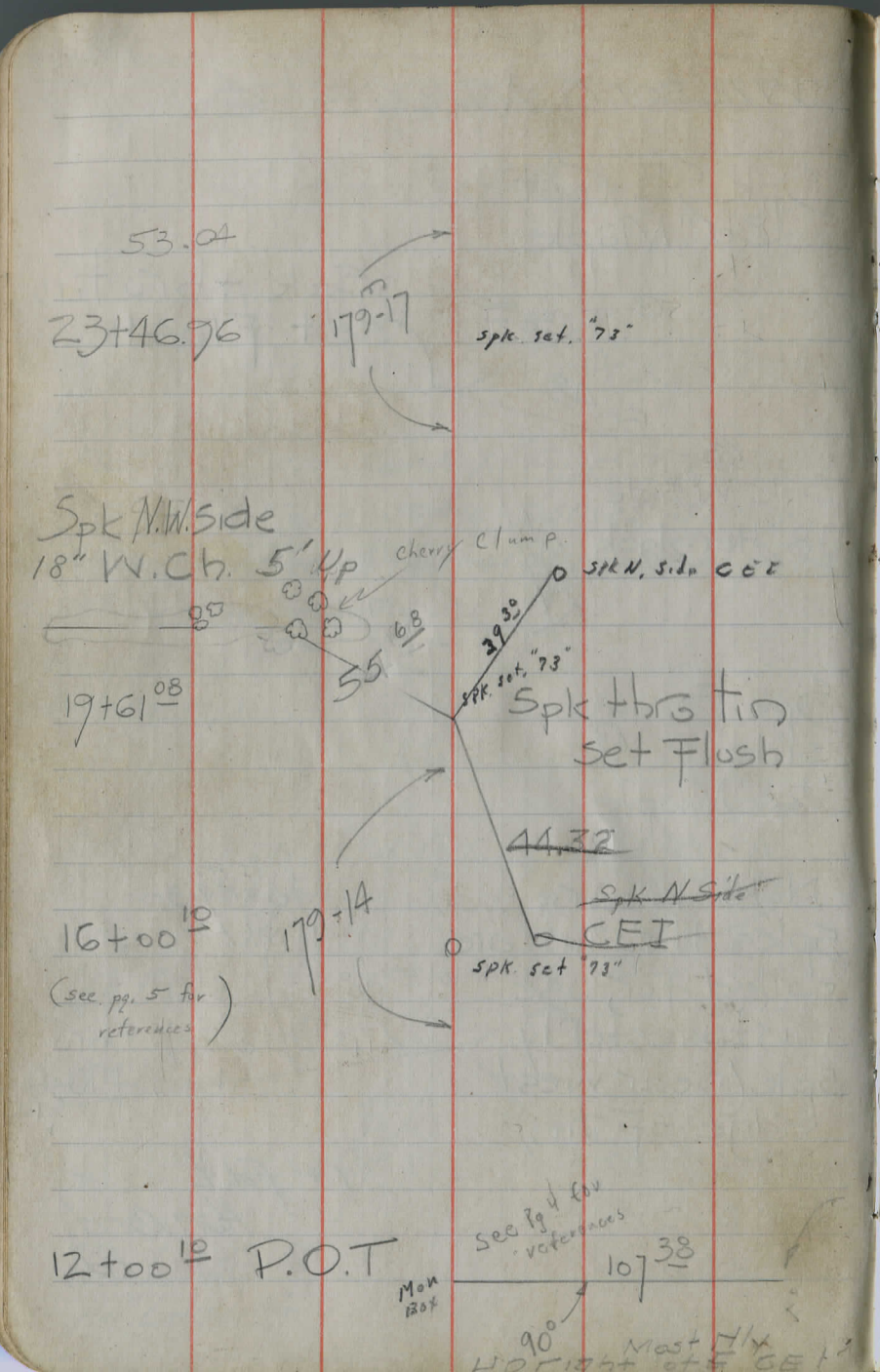


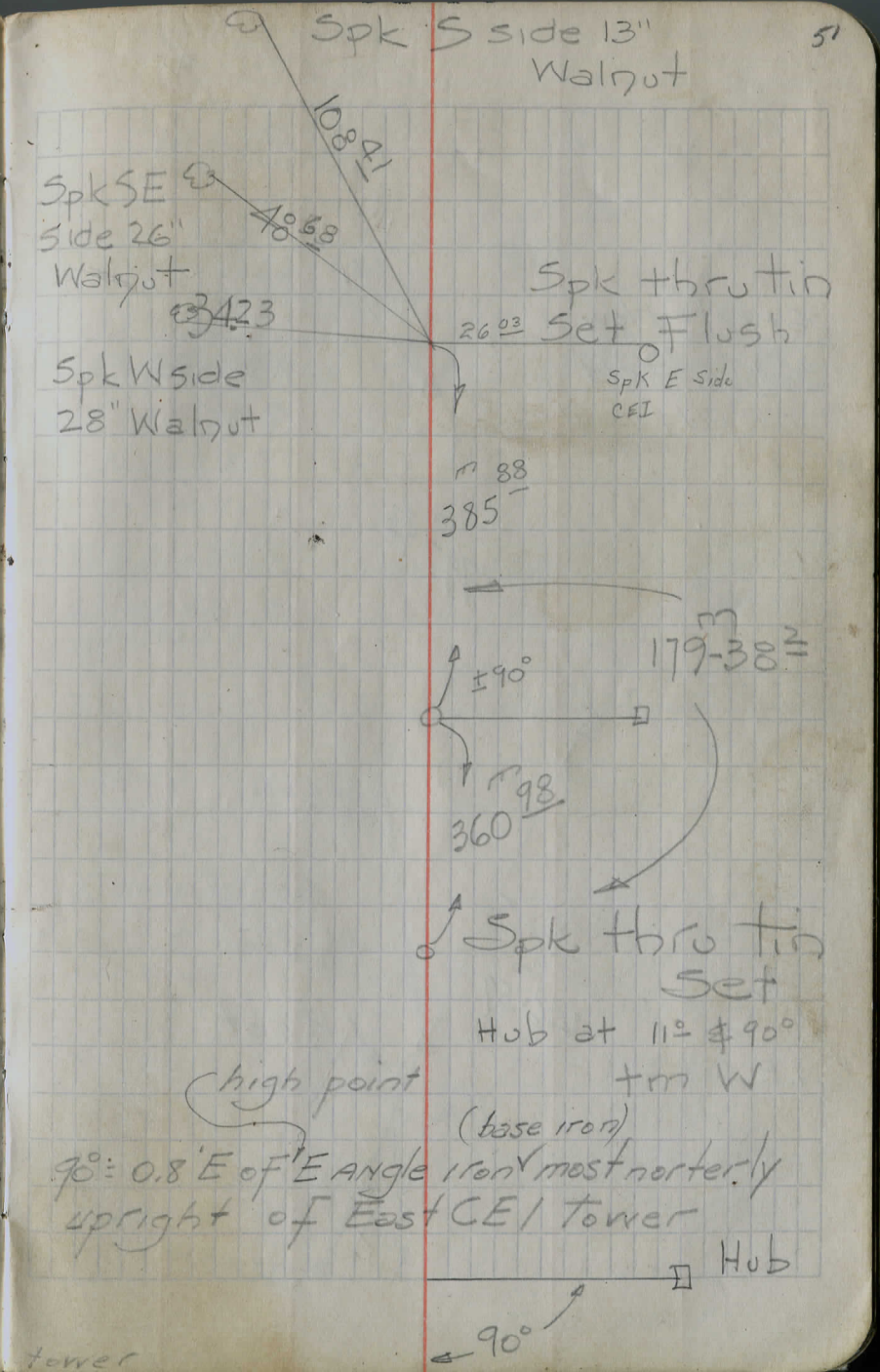
WILSON MILLS &

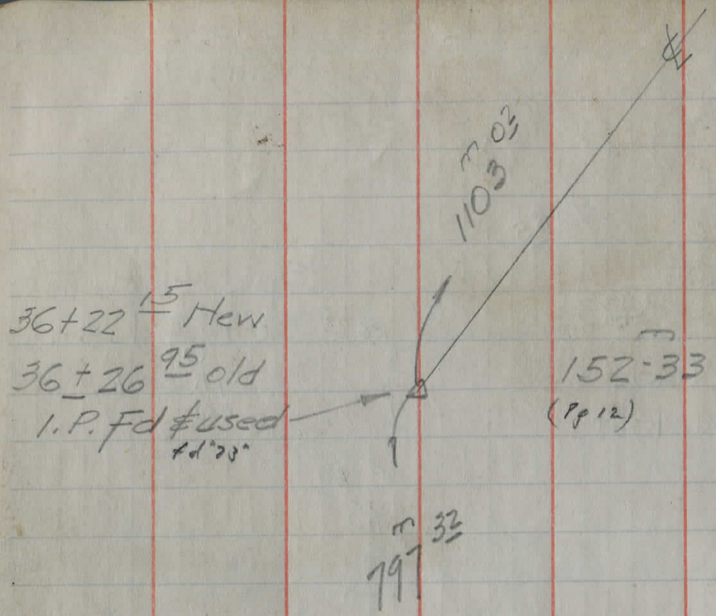


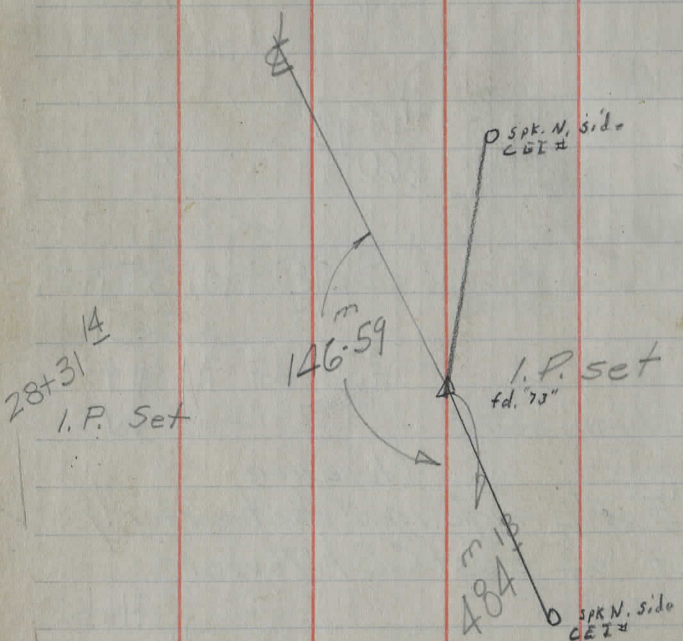
Note: Where Spks thru tin are called for, use most westerly Spk (near west edge of tin)

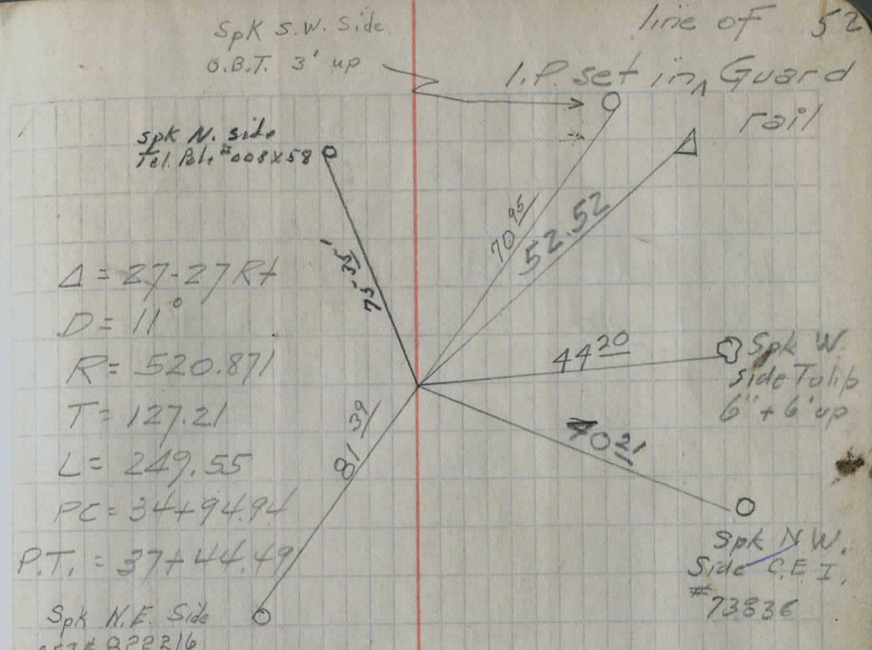



53.04
23+46.96
179-17
spk. set. "73"
Spk N.W. Side
18" W.Ch. 5' Up
cherry clump.
Spk N. Side CEI
39.30
55
68
spk. set "73"
19+61.08
Spk thru tin
set Flush
44.32
Spk N Side
CEI
179-14
16+00.10
spk. set "73"
(see pg. 5 for references)
12+00.10 P.O.T
see pg 4 for references
107.38
Mon Bolt
90°
Mast N/W
Upright of E CEI tower

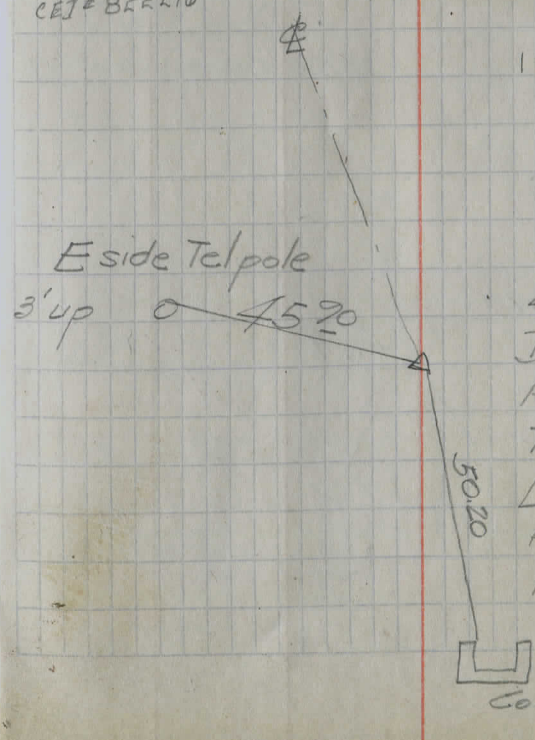

Spk S side 13"
Walnut
108.41
Spk SE
Side 26"
Walnut
40.68
34.23
Spk thru tin
26.03 Set Flush
Spk E Side
CEI
Spk W side
28" Walnut
88
385
179-38
±90°
98
360
Spk thru tin
Set
Hub at 11± & 90°
trm W
high point
(base iron)
90°± 0.8' E of E angle iron most northerly
upright of East CEI tower
Hub
90°







Δ = 27-27 Rt
D = 11°
R = 520.871
T = 127.21
L = 249.55
PC = 34+94.94
P.T. = 37+44.49



Δ = 33-01 Lt
D = 15°
R = 381.972
T = 113.21
L = 220.11
P.C. = 27+17.93
P.T. = 29+38.04

3.5' Ext

50+73 66 New
50±80.75 Old

173°21'

See pg 58 for correction

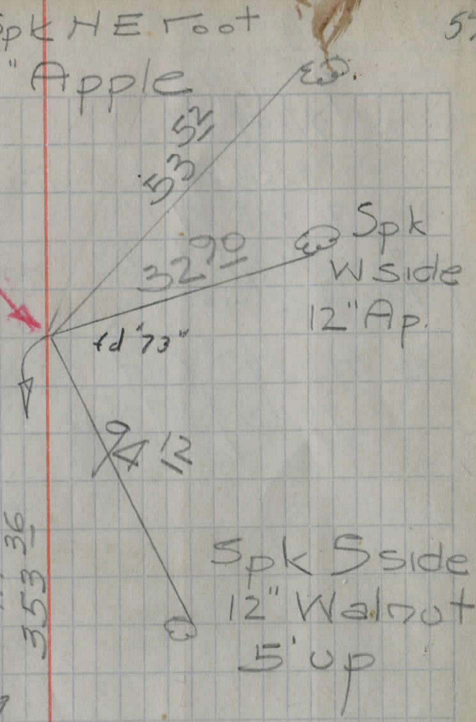
Spk thru tin set Flush

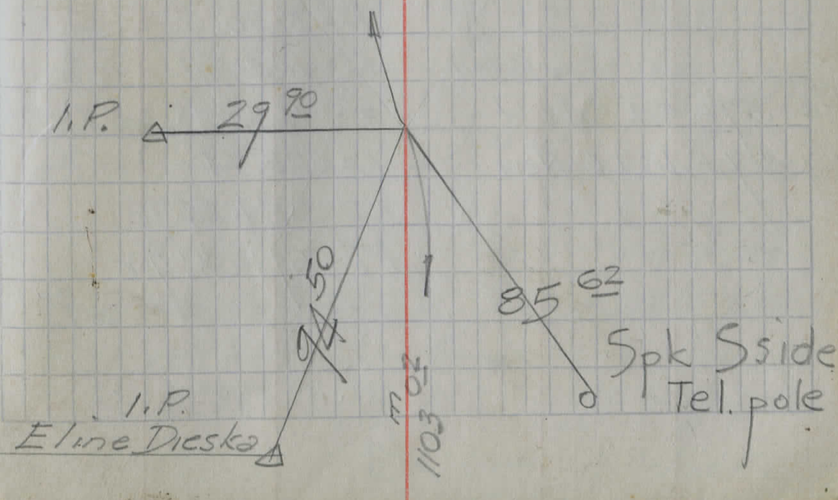
Corr of 0.55 H @ 36

47+20.30 New
47±26 91 Old

PoT

Hub 11.02 on
5 bisect
Δ = 6°39' Lt
D = 2°-45'
R = 2083.48
T = 121.05
L = 241.82
P.C. = 49+52.61
P.T. = 51+94.43
T on 11 offset = 121.69





Δ = 13-12-30 Rt
D = 7-30
R = 954.93
P.I = 77+49.37
T = 110.56 11' offset = − 1.27 = 109.27
PC = 76+38.81
L = 203.47
P.T = 78+42.28

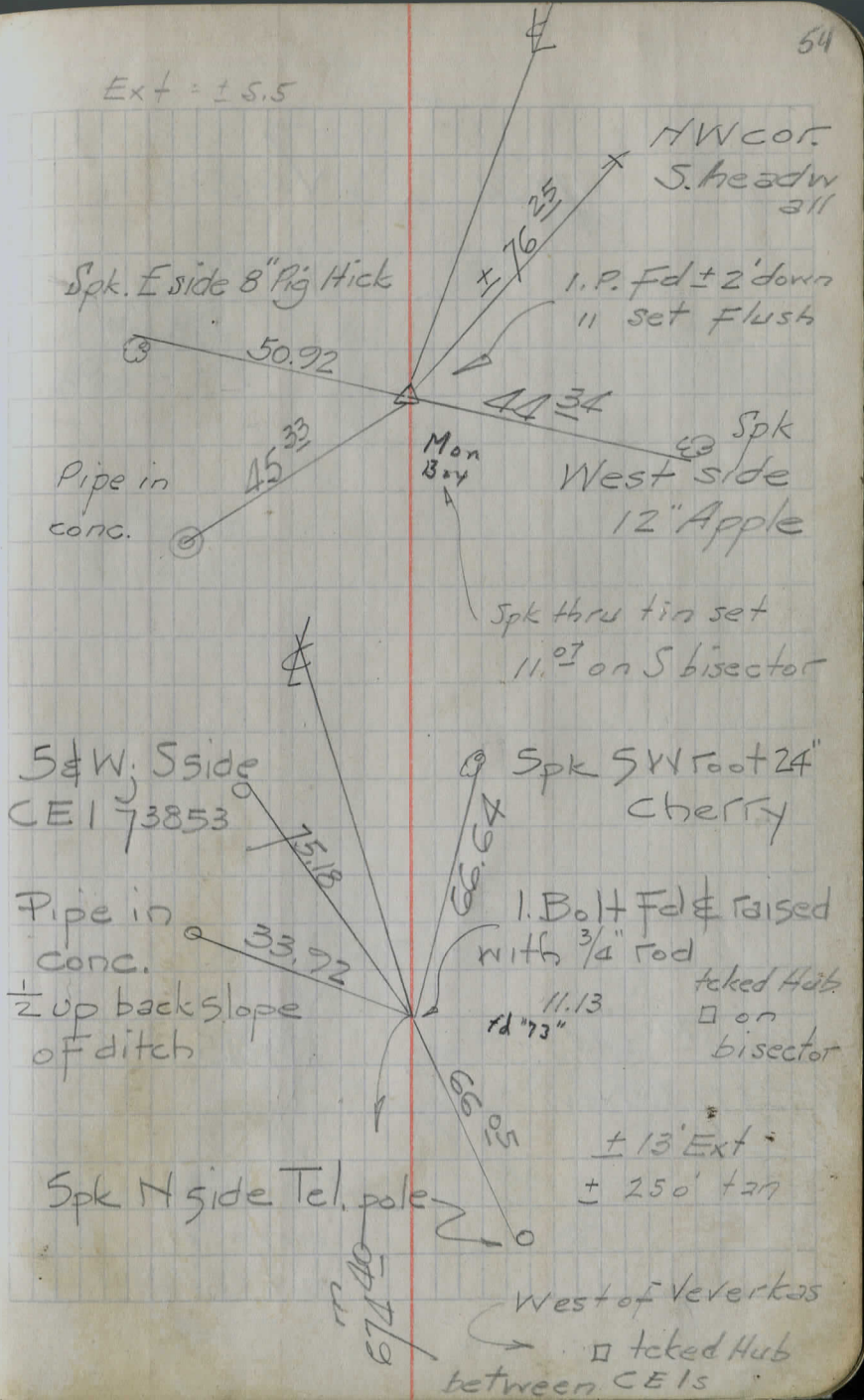
Sta. 77 ± 59.07 Old
" 77+49.37 New

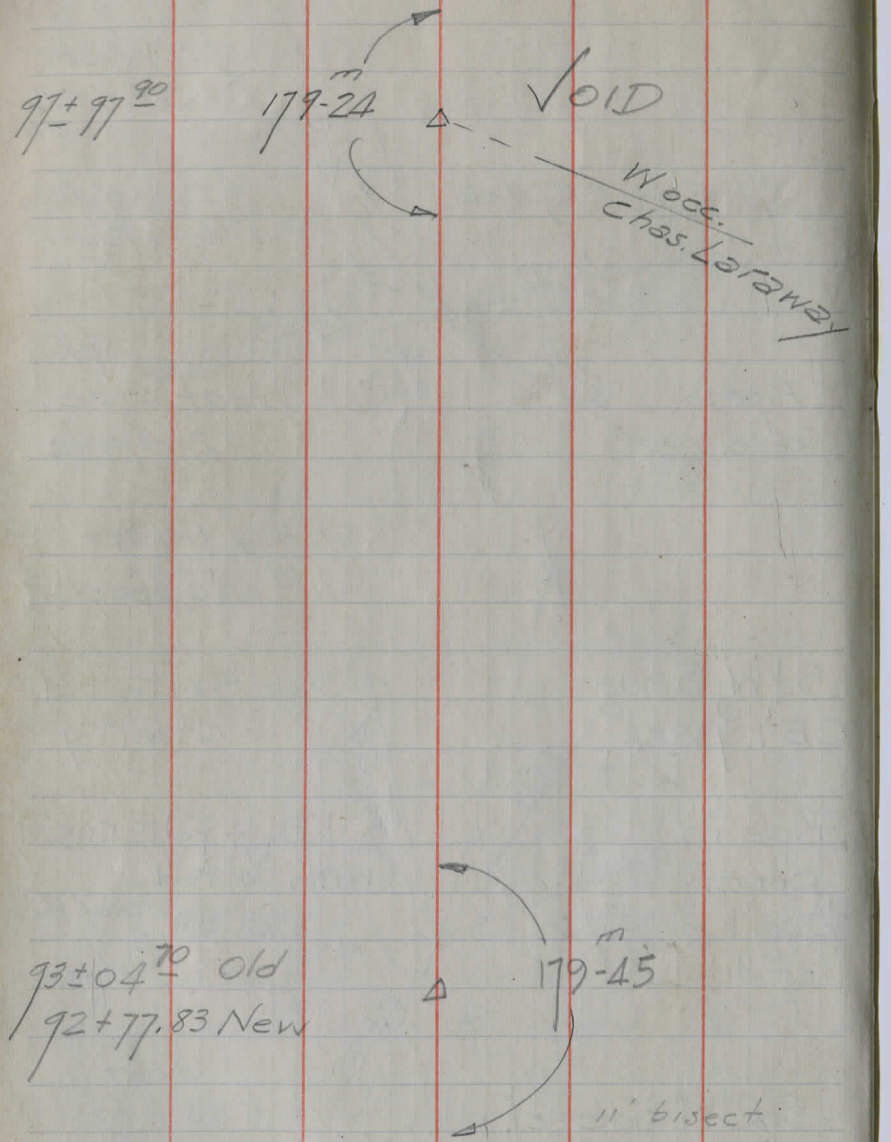
166-47-30 meas

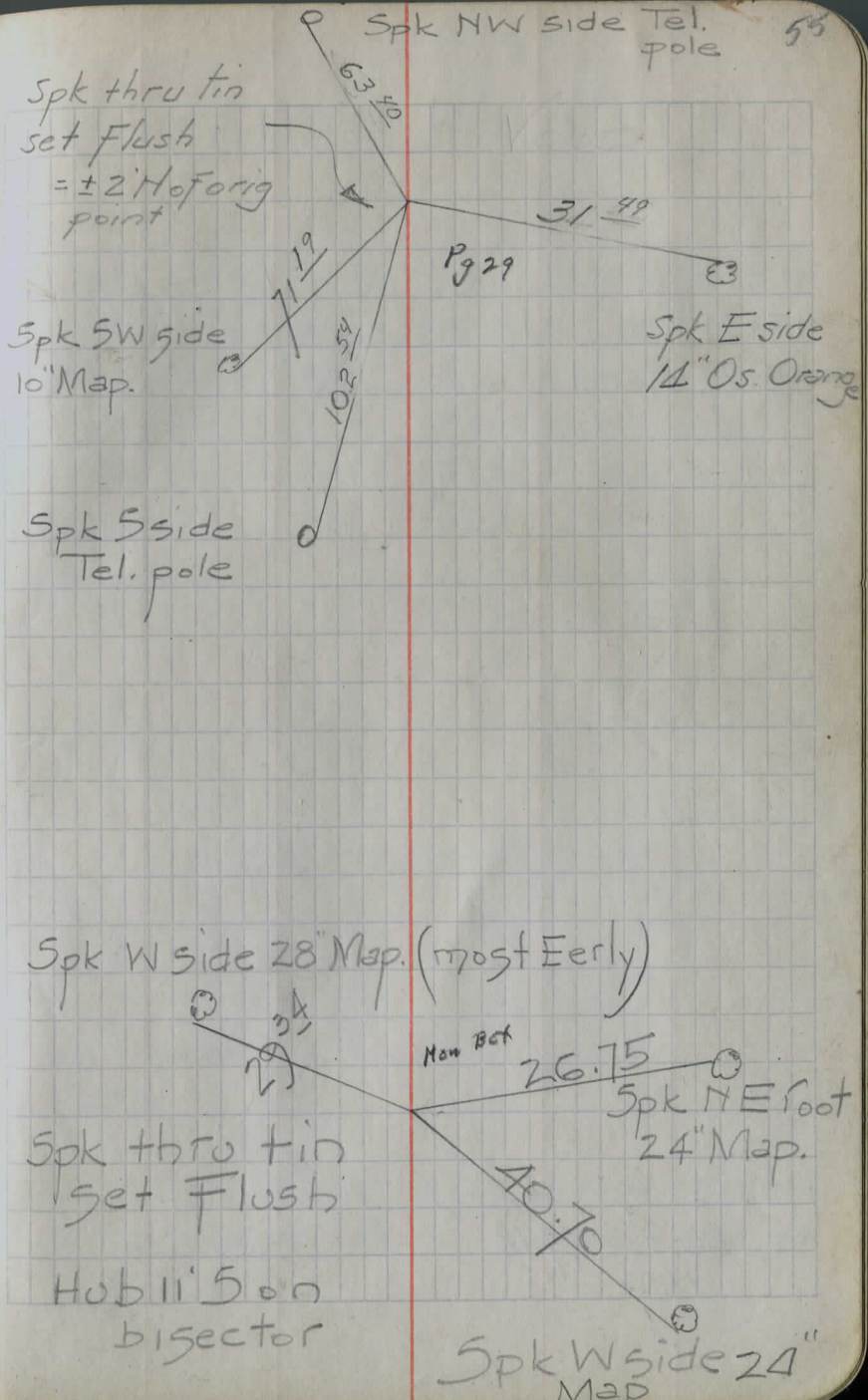
Δ = 17-49 Lt.
D = 5-30
R = 1041.741
T = 163.28 (11' offset 165.00)
L = 323.94
PC 55+84.78
PT 59+08.72

162-11

Sta. 57 ± 54.54 old
" 57+48.06 New




97+97.90
179-24
VOID
W occ.
Chas. Laraway
93+04.70 Old
92+77.83 New
179-45
11' bisect
corr = .07 one direction


Spk NW side Tel. pole
63 40
Spk thru tin set Flush
= ± 2' N of orig point
31 49
Pg 29
71 19
Spk SW side 10" Map.
102 54
Spk E side 14" Os. Orange
Spk S side Tel. pole
Spk W side 28" Map. (most Eerly)
34
Mon Bch
26.75
Spk NE Root 24" Map.
Spk thro tin set Flush
40.70
Hub 11'5 on bisector
Spk W side 24" Map

115+31.10 New
= 115+57.92 Old

? E Fowlers Mill Rd.

100+83.03 New

179.18

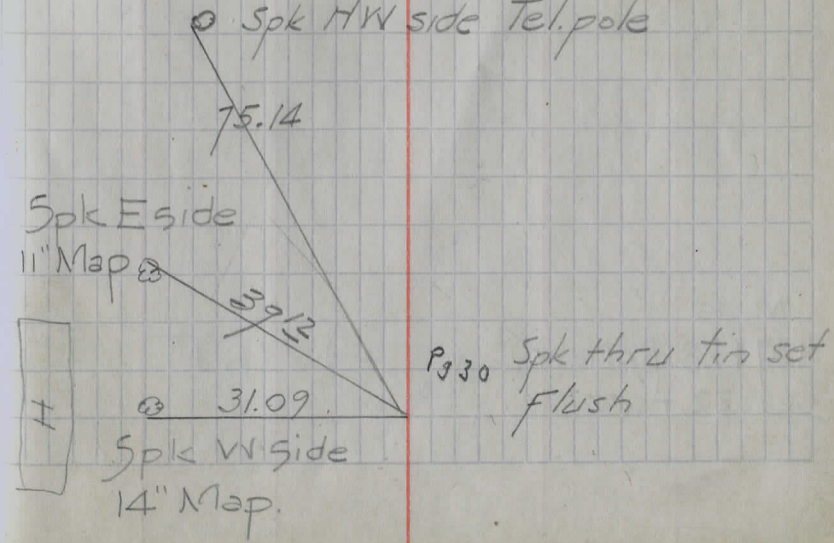
11 bis. corr = .07 one direction

See Refs. pg. 33

Mon Box

11 bis. corr
= 0.62 one direction

Δ = 18-55-30 Rt
D = 6°-30'
R = 881.474
P.I. = 115+31.10
T = 1 46.92
P.C. = 113+84.18
L = 2 91.15
P.T. = 116+75.33

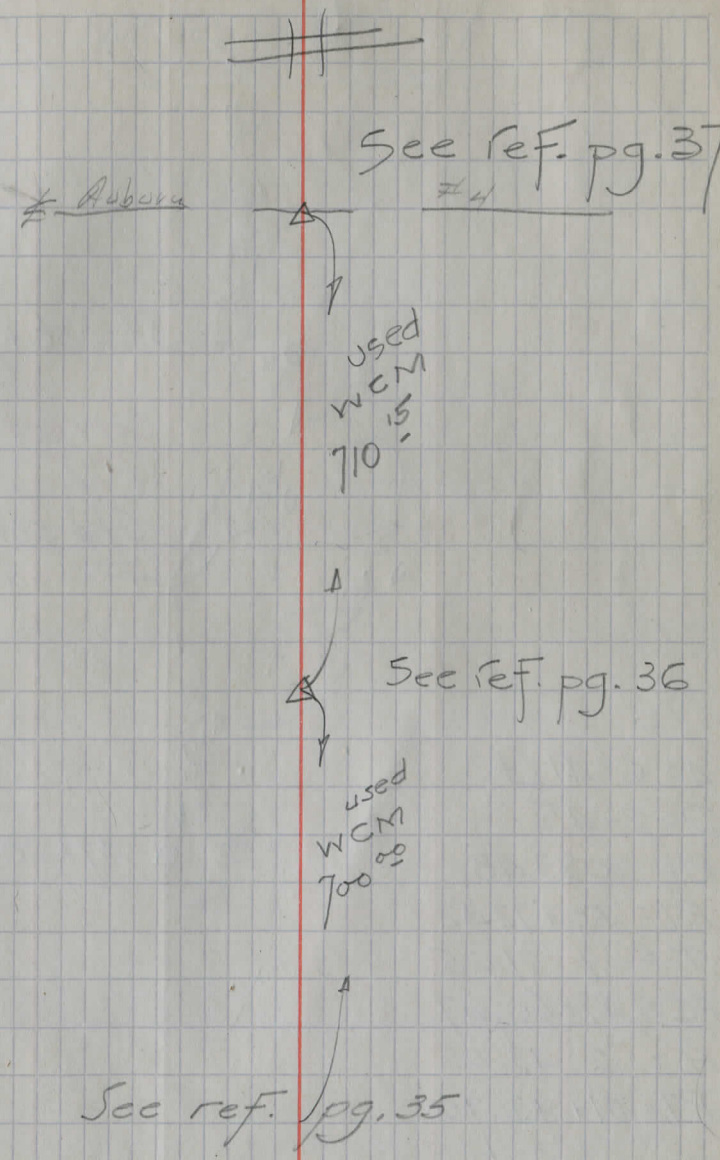


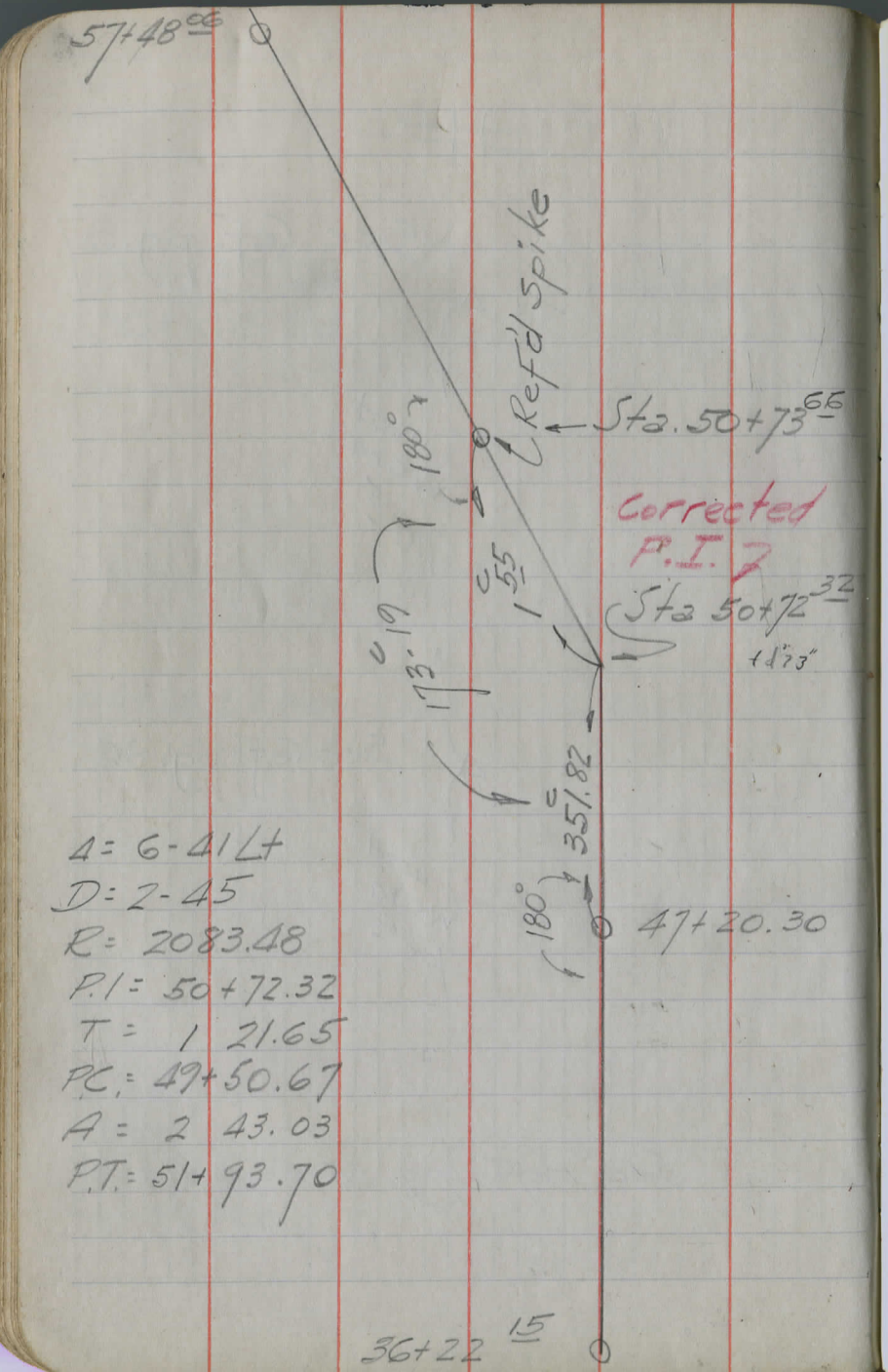
151+38.67 New
= 36+10.15 old

144+28.52 New
= Sta. 29+00 Old

Meas.
137+28.52 New
= Sta. 22+00

P.O.T



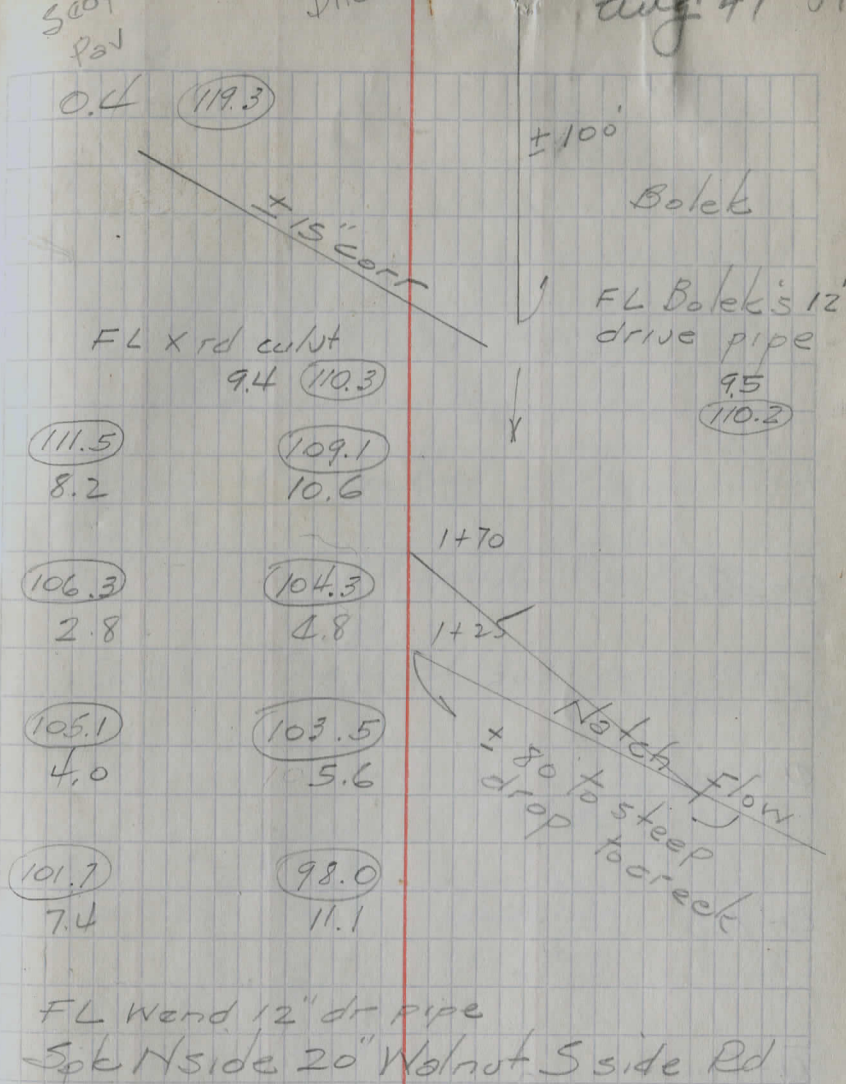


Δ = 6-41 Lt
D = 2-45
R = 2083.48
P.I = 50+72.32
T = 1 21.65
P.C. = 49+50.67
A = 2 43.03
P.T. = 51+93.70

3+0				
2+13 : 5 end X rd cul vt				
2+0				
T.P.	10.83	119.68	0.25	108.85
1+25				
1+0				
0+0				
			9.9	99.2
B.M.	9.10	109.10		100.00

0+0 = Line of fence E side Hallat's drive. Minus = West

Sedge Pav Ditch Aug 47 59



FL W end 12" dr pipe
Spk N side 20" Walnut S side Rd
0-25

N

-2 -1 0 1 2

WILSON MILLS RD.

no side rd ditch

2½'

±8' down slope

±10' down slope to ditch

Aug '47

Drive

Opp ditch badly eroded

HANKET.

John Hanket
13210 Melger Ave.
Cleve 20 Ohio

VEVERKA

15" corr.

12"

Not. Flow

Aug. '47

105

100

100 ft

South edge pavt

110.3 = F.L. X rd calvt

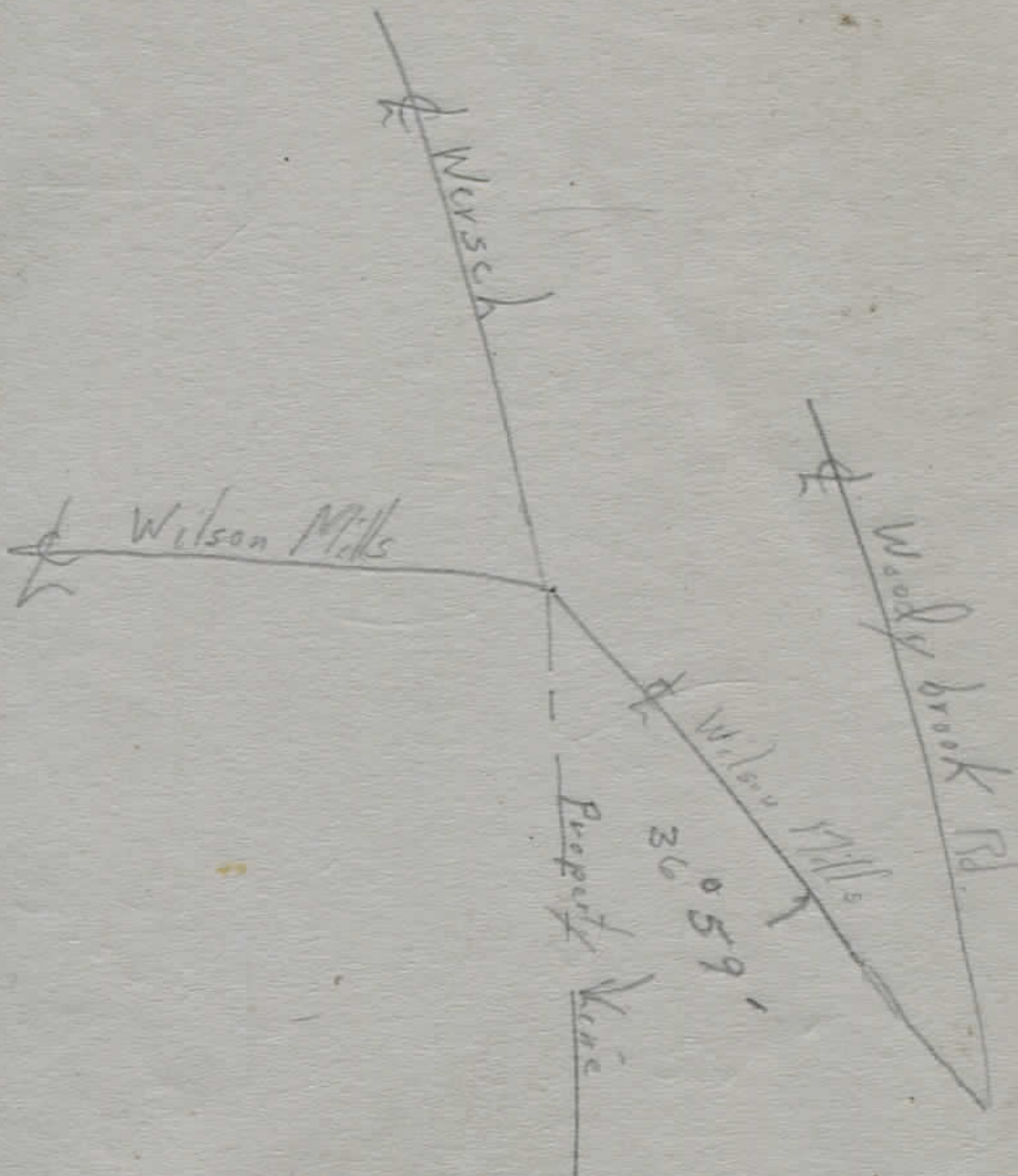
110.2 = F.L. Bolek drive pipe

Ed. ditch

F.L. (W. end) drive pipe

-3 -2 -1 0 1 2 3

Angle Between
℄ Wilson Mills & Property
Line across from Wersh Rd.



0-250			
0-200			
0-100			
0-50			
BM	3.38	103.38	100.00

S edge pabt

ditch south

No find x rd cubit to Boleks Ben Deska says old cubit eliminated

99.6
3.8

nord ditch 8' to down steep

0-225 no rd ditch sout side 10' to down step

99.0
4.4

97.2
6.2

0-198 ditch south

99.8
3.6

98.5
4.9

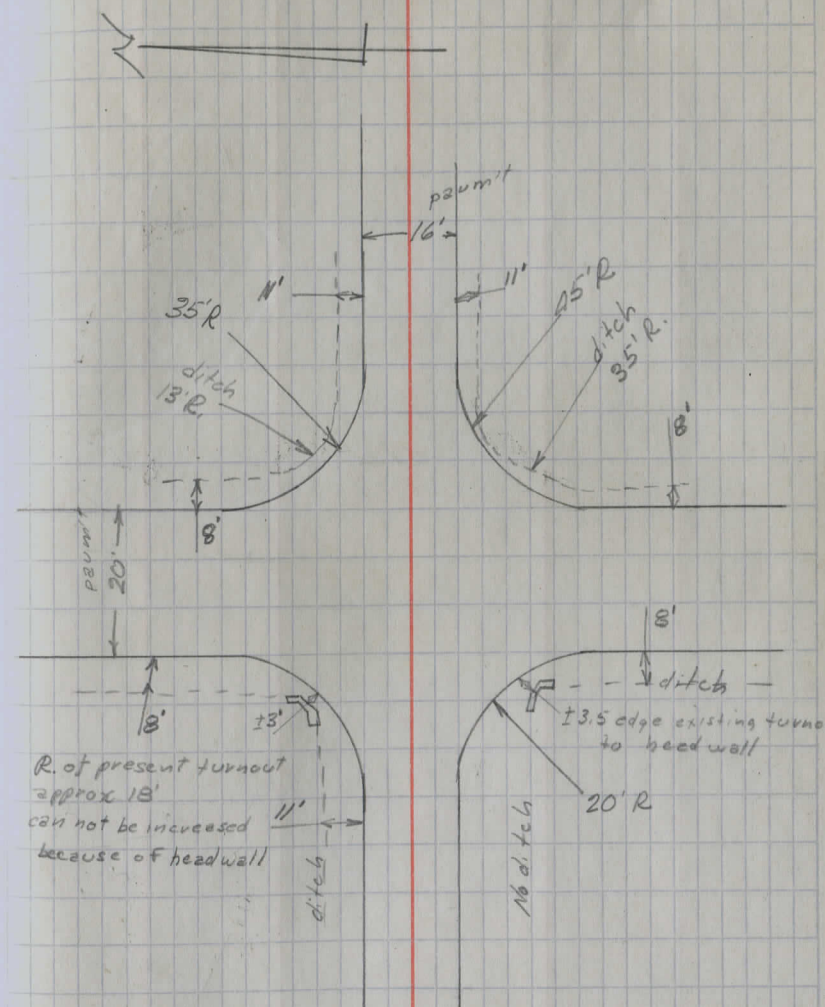
back slope ditch is higher than rd

100.5
2.9

99.0
4.4

Approx radius of Wheel track & ditches at int. Wilson Mills & 306

Sept '55



A. Temple
H. Patterson

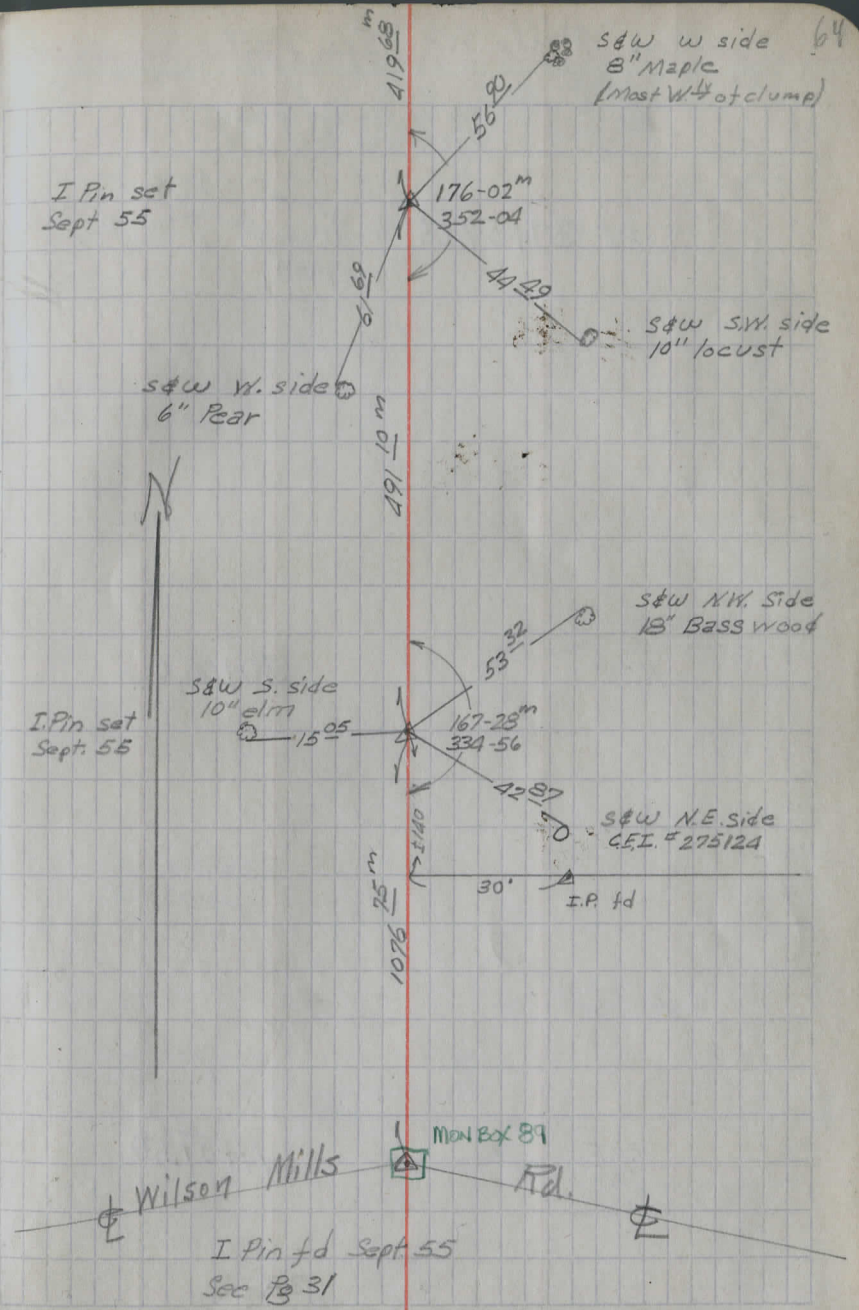
Survey Fowlers Mills Rd Sec. D-E

Sept. 55

PI 15+67.85

PI 10+76.75

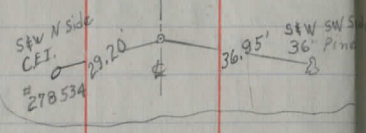
0+00



Fowlers Mills Rd See D-E

Pot

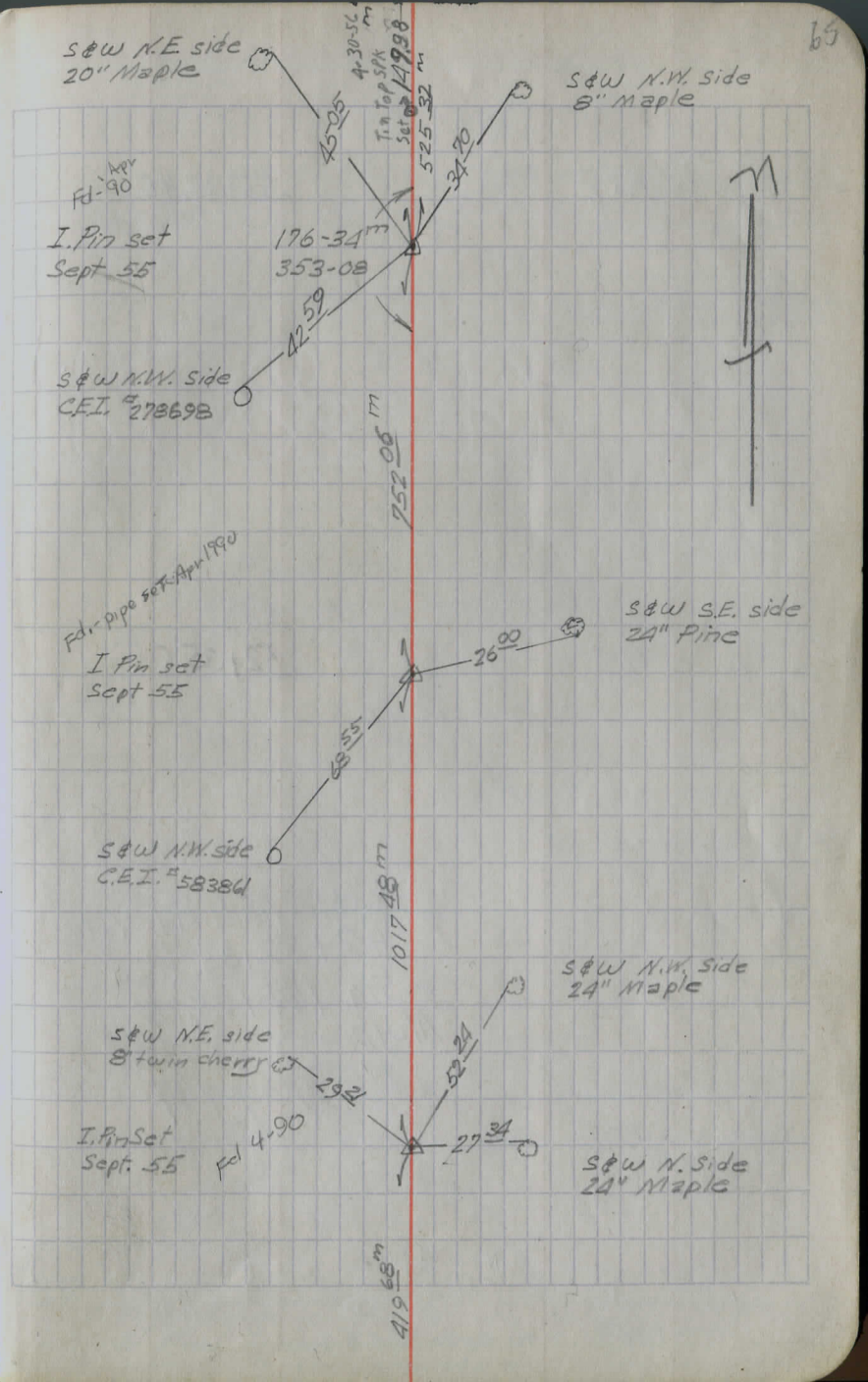
Tin Top SPK Set 4-30-56
249.98' S. of Intersection



P.I. 37+57.05

P.O.T. 30+05.0

P.O.T. 19+87.50

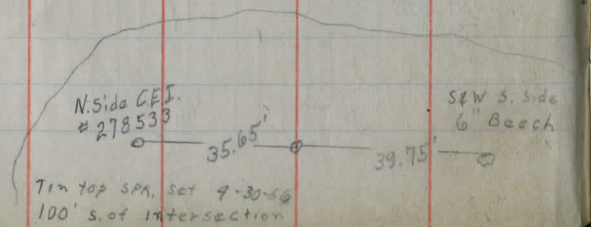


P.O.T. 55739.40

PI 52+35.05

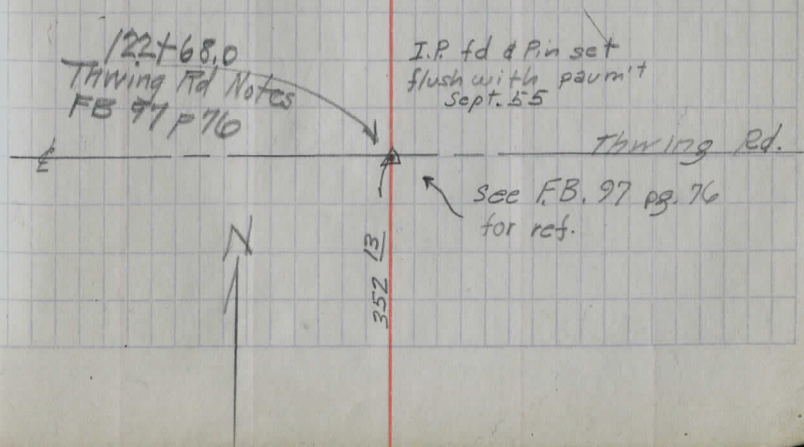
Fowlers Mills Rd. Notes
42+82.35
= Sta. 144+28.25
Mulberry Notes
FB 96 pg 67

P.O.T.



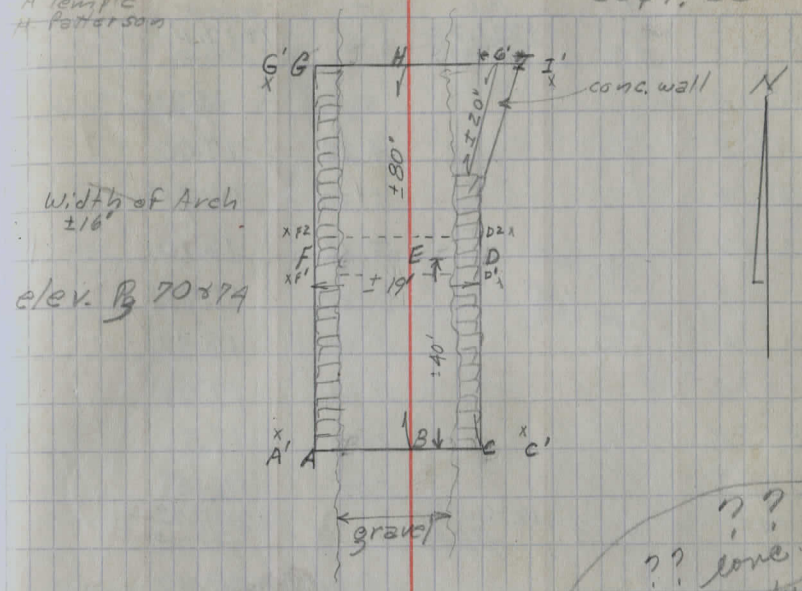
S&W S.E. side 15" Maple
352.13 m
46.27
S&W N. side 18" Maple
26.00
35.05
S&W S.W. side 20" Maple
I. Pin set Sept 55
I.P. Set Flush 11/2/56
304.35 m
S&W N.W. side 18" Maple
E = 4.0
T = ±100
45.22
169-50 m
339.44
19.4
S&W N. side 18" Maple
I. Pin set Sept. 55
I.P. Set Flush 11/2/56 JUNE '56
45.63
S&W S.W. side 18" Maple
1478.04 m
952.72
Fd-2 Apr 90 C 14" dN
123-56
347-52
I.P. fd. 11/2/56
℄ Mulberry Rd
322.41 m
25.43
S&W N. side 10" locust
35.00
83.28
See FB 96 Pg. 67
S&W N. side 12" Pine
4-30-56 Tin Top S.P.K. Set on line 100' S. of Int.
525.32 m
S&W E side 14" stem triple Basswood

58+91.50


122+68.0
Thwing Rd Notes
FB 97 P 76
I.P. fd & Pin set
flush with pavm't
Sept. 5-5
Thwing Rd.
℄
see F.B. 97 pg. 76
for ref.
N
352 13

Stone arch bridge over Moccasin Falls
Fowlers Mills Rd Sec. D
Sept. 55

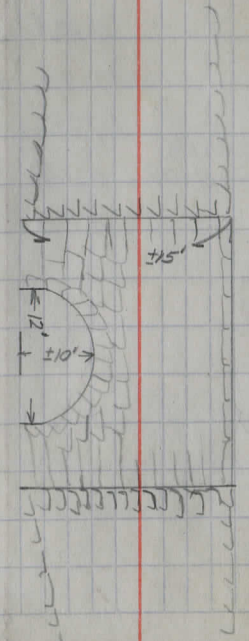
A Temple
H Patterson



Width of Arch ±16'

elev. BM 70.74

?? ??
?? conc. slab across structure & over hanging each side ?? ??



	+	HI	−	elev
BM	4.11	1221.22 ~~104.11~~		1217.11 ~~100.0~~
Point A			5.90	15.32
" B			4.22	17.00
" C			6.37	14.85
" D			5.12	16.10
" E			3.50	17.72
" F			4.90	16.32
" G			4.18	17.04
" H			2.70	18.52
" I			5.07	16.15
T.P.	0.44	1210.17 ~~93.06~~	11.49	1209.73 ~~92.62~~
			9.45	200.72
			9.43	00.74
			10.30	1199.43
			11.35	98.82
T.P.	11.45	1221.18 ~~104.07~~	0.44	1209.73 ~~92.62~~
B.M.			4.08	1217.10 ~~99.99~~

Sketch pg 69

Vert spk N root 24" Pine ± 30'S of Sand stone arch bridge ℄ ± 30' Rt $\overset{E}{\wedge}$ of ℄

Channel at E end of arch

± 20' E of E end of arch channel at W end of arch

± 20' W of W end of arch where falls starts

A. Temple
H. Patterson

B.M. Levels from The int. of Auburn & Thwing Rd to Maccosin falls bridge

Sept. 65

	+	HI	−	elev	
B.M.(a)	3.20	59.02		1255.82	
T.P.	0.78	48.11	11.69	47.33	
T.P.	0.73	39.42	9.42	38.69	
T.P.	10.91	49.18	1.15	38.27	
T.P.	11.78	60.65	0.31	48.87	
T.P.	10.93	71.02	0.56	60.09	
T.P.	9.73	80.49	0.26	70.76	
B.M.(b)			4.60	1275.89	use
T.P.	0.13	74.92	5.70	74.79	
T.P.	0.40	64.29	11.03	63.89	
T.P.	0.22	53.09	11.42	52.87	
T.P.	0.55	42.59	11.05	42.04	
T.P.	1.56	33.78	10.37	32.22	
T.P.	0.20	22.26	11.72	22.06	
B.M.(m)			5.15	1217.11	use

Check levels back to starting Point

B.M.(m)	5.15	22.26		1217.11	
T.P.	11.35	33.41	0.20	22.06	
T.P.	9.99	42.23	1.17	32.24	
T.P.	10.92	52.97	0.18	42.05	
T.P.	11.35	64.23	0.10	52.87	
T.P.	11.23	75.14	0.32	63.91	
T.P.	5.20	80.15	0.19	74.95	
B.M.(b)			4.25	1275.90	

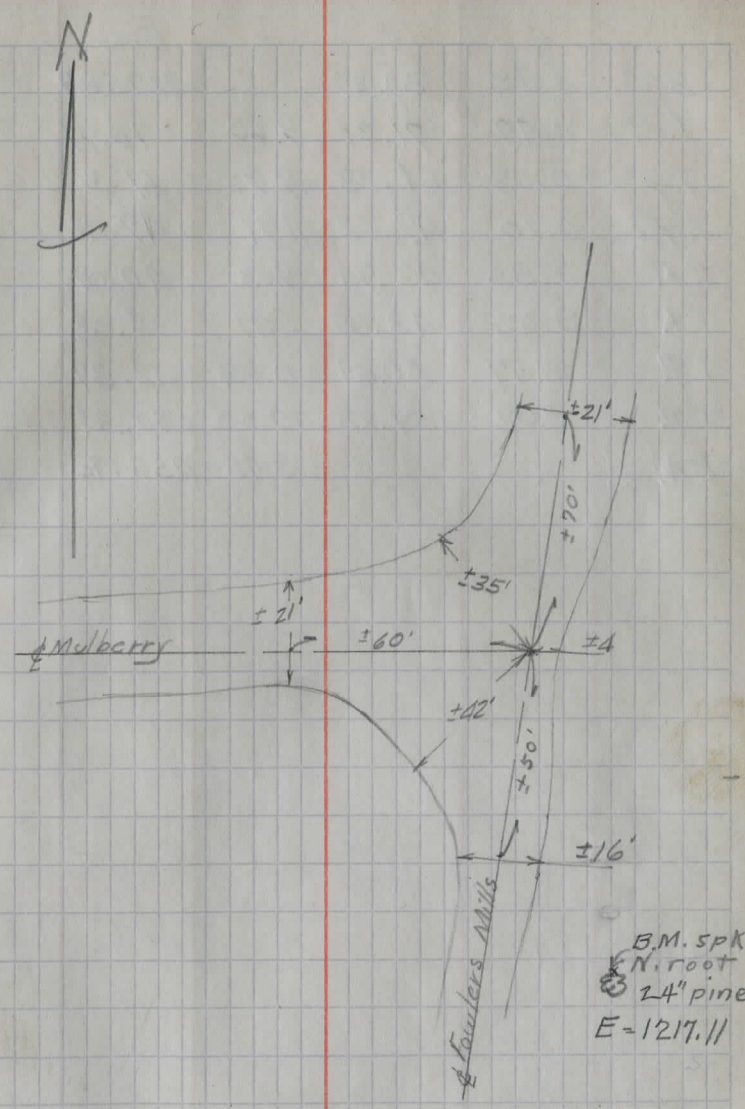
continued Pg 73

Vert Spk E root 16" Maple ±26' S of Auburn & Thwing Rd int. 30' Rt. (E) ∧ Auburn Rd ℄

Vert spk NW side 15" Maple ±33' E. of Thwing ℄ Fowlers Mills Rd. int. ±25' Rt. S ∧ of Thwing Rd. ℄

Vert spk N root 24" Pine ±30' S of S end stone arch bridge ±30' Rt. E ∧ of ℄ of Fowlers Mills Rd.

Traveled Rd. with respect to ℄ 7



	+	HI	−	Elev.
BM	4.48	80.37		1275.89
T.P.	0.49	71.26	9.60	70.77
T.P.	0.03	61.33	9.96	61 30
T.P.	0.20	49.62	11.91	49.42
T.P.	0.85	40 .94	9.53	40.09
T.P.	8.02	43.05	5.91	35.03
T.P.	8.47	50.84	0.68	42.37
T.P.	8.89	59.23	0.50	50.34
B.M. (c)			3.45	1255.78

	+	HI	-	ELEV.	
B.M.	4.20	1221.31		1217.11	
Point A			6.01		
B			4.27		
C			6.49		
D			4.99		
E			3.59		
F			5.86		
G			4.25		
H			2.65		
I			5.08		
T.P.	1.97	1219.51	8.77	1212.54	
Point A'			8.73		-1' to bedrock
TP	8.87	1214.65	8.97	1205.78	
Point C'			9.28		-8" to bedrock
TP	11.36	1203.30	11.71	1202.94	
Point D'			8.56		
E'			9.00		
I'			.68		-5' to bedrock
TP F'	5.16		8.56		
TP + F'	10.28	1207.34	6.84	1197.06	
~~TP~~	~~.48~~		12.46		
Point G'			~~11.08~~	1209.88	-1' to bedrock
TP	.45	71	11.08	1196.26	
BM			9.48		

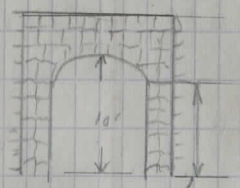
Elev. Moccasin Falls bridge

Patterson
Canfield
Heller
4-28-56

See Pg 69

B.M.	4.20	1221.31		1217.11
A			6.01	15.30
B			4.27	17.04
C			6.49	14.82
D			4.99	16.32
E			3.59	17.72
F			5.26	16.05
G			4.25	17.06
H			2.65	18.66
I			5.08	16.23
TP	1.97	1214.51	8.77	1212.54
A'			8.73	1202.88
TP	8.87	1221.41	1.97	1212.54
C'			9.28	12.13
TP	.36	1210.06	11.71	1209.70
D'			8.56	1201.50
D^2			9.00	1201.06
I'			.68	1209.38
TP - F^2	5.16	1206.66	8.56	1201.50
TP - F'	10.28	1210.10	6.84	1199.82
G'			2.46	1207.64
TP	11.88	1221.73	.45	1210.65
BM			4.48	1217.25

± 1.5' Dirt on top of bridge



Dist from foundation to begining of curve of Arch

E. end 4.8'
W. end 4.5'

-1' to bedrock

-8' to bedrock

± 10' out from Present bridge Walls
Refer to Picture Pg. 69 this Book

-5' to bedrock

-1' to bedrock

℄ Elev Fowlers Mill Rd 5-9-56
500' Nes of Stone Arch bridge Patterson Heller

	+	HI	−	Elev
BM	3.90	1221.01		1217.11
100' S.			5.11	1215.90
200' S.			2.42	1218.59
T.P.	6.88	1227.84	.05	1220.96
300' S.			5.35	1222.49
400' S			9.30	1223.54
500' S			4.30	1223.54
T.P.	10.65	1227.98	10.51	1217.33
100' N.			6.90	1221.08
200' N.			.71	1227.27
T.P.	8.14	1235.40	.72	1227.26
300' N.			6.30	1229.10
400' N.			4.46	1230.94
500' N.			2.80	1232.60
T.P.	.03	1223.92	11.51	1223.89
			7.01	1216.91

ELEVATIONS FOR E. SIDE N. END OF MOCASSIN FALLS BRIDGE

Sta	+ B.S.	HI	− F.S.	Elv
B.M	5.95			100.00
		105.95		
~~1~~	~~6.95~~			
1			5.54	100.41
2			5.85	100.10
3			5.14	100.81
4			5.41	100.54
5			4.74	101.21
6			4.60	101.35
7			6.27	99.68
8			7.83	98.12
9			9.05	96.90
TP1	1.14		13.16	92.79
~~TP1~~		93.93		
10	~~9.26~~		9.26	84.67
11	~~10.33~~		10.33	83.60
12	~~10.58~~		10.58	83.35
TP-2	10.95		1.92	92.01
		102.96		
B.M.			2.98	99.98
				-0.02

J.A.C.
G.A.M.
J.A.C.

WARM, HUMID, CLOUDY 78°F
31 AUG 81

77

Remarks

X cut in conc retaining wall SW cor.

E. edge of pavement STa 00
" " STa 0+11
E. edge of pavement STa 0+21 3
" " 0+29 2
" " 0+37 6
" " 0+43 8
Ground Elevations 12'ff 9 0+43 8
" " 0+37 6
" " 0+31
0+19 CORNER of ROCK

GROUN ELEV 0+19 (~~ROCK OUTCROP~~)
Rock out crop N. edge of Arch
" " " S. edge of Arch

* GROUND ELEV ARE 12' E. of traveled rd.

* ROAD STA PROCEED NORTH 0+00 @ ℄ ARCH

ELEVATION FOR W. SIDE N. END
MOCASSIN FALL

STA	BS +	HI	FS −	ELEV
Bm	7.12	~~107.12~~		100.00
		107.12		
1			5.86	101.26
2			5.96	101.16
3			5.74	101.38
4			5.57	101.55
5			5.33	101.79
6			5.24	101.88
7.			7.38	99.74
8.			12.48	94.64
TP-1	0.22		10.30	96.82
9		97.04	5.21	91.83
10			8.57	88.47
11			10.28	86.76
12			11.58	85.46
13			12.06	84.98
14			13.29	83.75
TP-2	12.76		3.22	93.82
		106.58		
BM			6.57	100.01

(+.01)

F JAC
/ GAM
T JAC.

PARTLY CLOUDY
WARM HUMID
1 SEP 81

REMARKS

X CUT SW CORNER TO W SIDE of ROAD CONC RETAINING WALL

STA 0+00 W. EDGE PAVM't
" 0+11 W. EDGE PAVM't
" 0+21.3 " " "
" 0+29.9 " " "
" 0+37.6 " " "
" 0+43.8 " " "
0+43.8 Grd.
0+37.6 "

0+29.9 Grd
0+21.3 " --

Rock out crop 22' off ℄ ~~Same~~ STA 0+21.3
STA 0+11 Bottom of grade - Bed Rock
N. edge of Arch - Bed Rock
S. edge of Arch - " "

Road STA Proceed N. Ground elevations
0+00 @ ℄ Arch 10' W of ℄ of Pavement
(TRAVELED ROAD)

8-5-37

Culvert 6+51

	+	H.I.	−		
BM #2	0.16	1270.63			1270.47
			11.04	1259.59	
	4.34	1263.93			
So.			R 7.68	1256.25	Fl. So
No.			R 7.0	1256.93	" No

Culv. 16+16

BM #3	4.75	1290.65		El = 1285.93
			8.9	
So			R 10.10	1280.55
No			R 9.30	1281.35

7+56 E nail measd from 0+0 line between 0+0 & ~~75+~~ ± 12+00[10]

W nail from ± ref

W nail 0.20 So of line

& 0.81 W of E nail

Roberts Wilsons Millsed. 79

Graber Records Daily Class.

Cut 1.5 30' off ℄

" 2.5 30' "

1200.10
756.57
443.53

Grade 35' off "

Cut 3.5 35' " "

12+00[10] = W tack = ref

℄ tack meas'd

5748.06
163.28
5584.78
323.94
5908.72

KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P.=23° 20′ to the R. at Station 542+72.

Ext. in Tab. IV opposite 23° 20′=120.87
120.87÷12=10.07. Say a 10° Curve.

Tan. in Tab. IV opp. 23° 20′=1183.1
1183.1÷10=118.31.

Tab. V. correction for A. 23° 20′ for a 10° Cur.=0.16
118.31+0.16=118.47=corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. 23° 20′=23.33°÷10=2.3333=L. C.

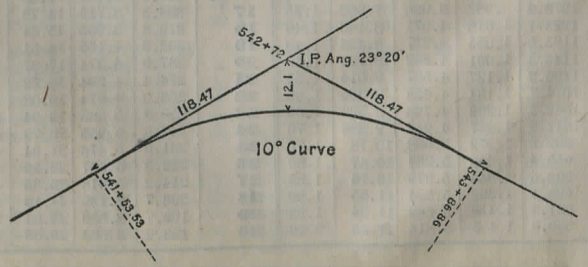
2° 19½′=def. for sta.	542	I. P.=sta.	542+72
4° 49½′= " " "	+50	Tan.=	1.18.47
7° 19½′= " " "	543	B. C.=sta.	541+53.53
9° 49½′= " " "	+50	L. C.=	2.33.33
11° 40′= " " "	543+	E. C.=sta.	543+86.86
	86.86		

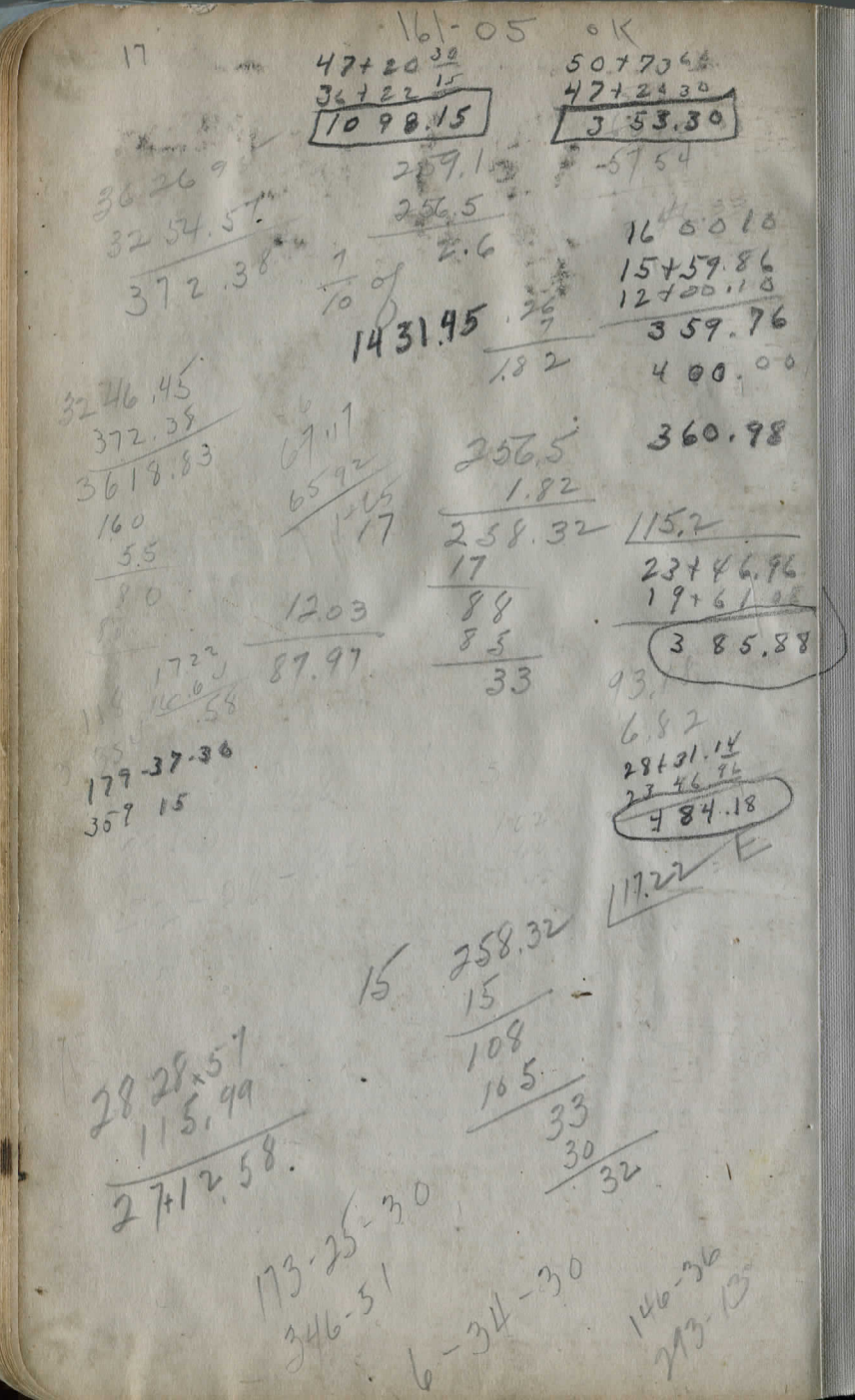
100—53.53=46.47×3′(def. for 1 ft. of 10° Cur.)=139.41′=2° 19½″=def. for sta. 542.

Def. for 50 ft.=2° 30′ for a 10° Curve.

Def. for 36.86 ft.=1° 50½′ for a 10° Curve

(These tables are published in Field Books of KEUFFEL & ESSER Co., New York, N. Y.)





PLEASE RETURN TO GEAUGA COUNTY ENGINEER COURT HOUSE CHARDON, O. PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SCIENCE TRACK ENGINEERS.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

R.